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(71) Applicant (for all designated States except US): **DO-COMO COMMUNICATIONS LABORATORIES EUROPE GMBH** [DE/DE]; Landsberger Strasse 308-312, 80687 München (DE).

(72) Inventor; and

(75) Inventor/Applicant (for US only): **AUER, Gunther** [DE/DE]; Westendstrasse 51, 80339 München (DE).

(74) Agents: **SCHOPPE, Fritz** et al.; Schoppe, Zinttermann, Stöckeler & Zinkler, Postfach/P.O. Box 246, 82043 Pullach bei München (DE).

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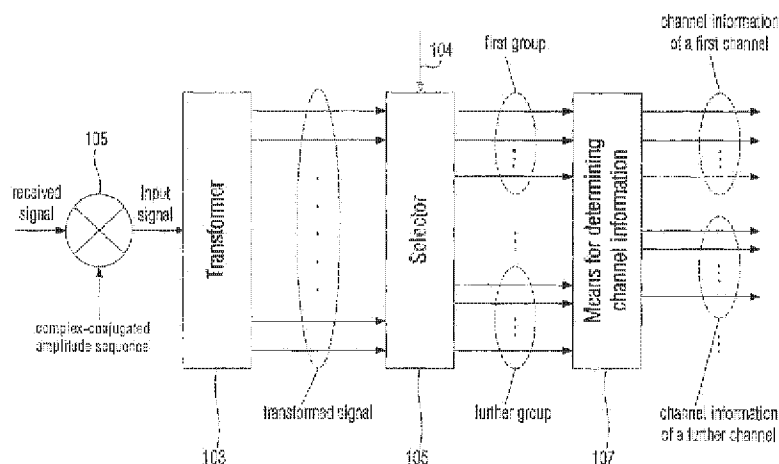
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(54) Title: APPARATUS AND METHOD FOR ESTIMATING A PLURALITY OF CHANNELS



(57) Abstract: An apparatus for estimating a plurality of channels from a plurality of distinct transmitting points, wherein an input signal includes a superposition of signals based on a first pilot sequence transmittable from a first transmitting point and on a second pilot sequence transmittable from a second transmitting point, the first pilot sequence and the second pilot sequence having a phase shift to each other, comprises a transformer (103; 303), which is operative to translate phase shifts between the first and the second pilot sequence into a delay, so that a first group of a set of discrete values of the transformed signal includes channel information of a first channel and that a second group of a set of discrete values includes channel information of a second channel, a selector (105; 305) for selecting the first group from the set of discrete values and for selecting the second group from the set of discrete values to obtain selected groups, and means (107; 315) for determining channel information for the plurality of channels based on the selected groups. The selection of groups at the output of the transformer for obtaining channel information for the channel allows the construction of a simplified receiver.

**Apparatus and Method for Estimating a Plurality of Channels**Description

The present invention is in the field of telecommunications and, in particular, in the field of channel estimation in a multiple input scenario, in which a receiver receives signals from more than one transmitting antennas.

The steadily-increasing demand for high data rates necessary for today's and future mobile radio applications require high data rate techniques efficiently exploiting the available band width or, in other words, the achievable channel capacity. Therefore, multiple input multiple output (MIMO) transmission systems have achieved considerable importance in recent years. MIMO systems employ a plurality of transmitting points, each of the transmitting points having a transmit antenna, and a plurality of receiving points, each of the receiving points having a receiving antenna, to receive signals being transmitted by the multiple transmitting points through different communication channels. In MIMO techniques, where the signals impinging from several transmitter antennas need to be separated, space - time codes or special multiplexing methods are used.

The signals impinging on each receive antenna are the super-position of the signals from  $N_T$  antennas, where  $N_T$  denotes a number of transmitting points. This implies new challenges for channel estimation. Channel parameters, like a channel impulse response or a channel transfer function are required for subsequent processing of the received

5 data. While the separation of the signals corresponding to several transmitting points, each of them having a transmit antenna, is a challenging task, the extension from a receiver having one antenna to a system with several receive antennas is straight forward, as long as the  
10 signals are mutually uncorrelated. The structure of the channel estimation units is independent of the number of receive antennas  $N_R$ . The extension from a multiple input single output (MISO) system to a MIMO system is to employ  $N_R$  parallel channel estimation units, one for each  
15 receiving point (receive antenna).

The use of coherent transmission techniques in wireless systems requires estimation and tracking of the mobile radio channel. Since the signals transmitted from multiple  
20 transmit antennas are observed as mutual interference, channel estimation for MIMO systems is different from the single transmit antenna scenario. MIMO systems can be used with a multi-carrier modulation scheme to further improve the communication capacity and quality of mobile radio  
25 systems. A prominent representative of multi-carrier modulation techniques is the orthogonal frequency division multiplexing (OFDM) technique. A block diagram of an OFDM system is shown in Fig. 7.

30 Multi carrier modulation in particular orthogonal frequency division multiplexing (OFDM) has been successfully applied to a wide variety of digital communication systems over the past several years. In particular for the transmission of large data rates in a broadcasting scenario (e.g. digital  
35 TV), OFDM's superior performance in transmission over dispersive channels is a major advantage. OFDM has been chosen for various digital broadcasting standards, e.g. DAB

5 or DVB-T. Another wireless application of OFDM is in high speed wireless local area networks (WLAN).

OFDM was first introduced in the 1960s. An efficient demodulation utilising the discrete Fourier transform (DFT)  
10 was suggested by S. Weinstein and P. Ebert, "Data Transmission by Frequency Division Multiplexing Using the Discrete Fourier Transform", IEEE Transactions on Communication Technology, vol. COM-19, pp. 628-634, Oct. 1971. By inserting a cyclic prefix into the guard interval  
15 (GI) longer than the maximum delay of the channel, inter-symbol interference (ISI) can be eliminated completely and the orthogonality of the received signal is preserved. Since future mobile communication systems should support data rates several times higher than current systems,  
20 multi-carrier systems with proper coding and interleaving offer both efficient implementation through the application of the Fast Fourier Transform (FFT) and sufficient robustness to radio channel impairments.

25 Another OFDM-based approach, termed multi-carrier code division multiplex access (MC-CDMA), were spreading in frequency direction as has been introduced in addition to the OFDM modulation, as described in K. Fazel and L. Papke, "On the Performance of Convolutionally-Coded CDMA/OFDM for  
30 Mobile Communication Systems", in Proc. IEEE Int. Symposium on Personal, Indoor and Mobile Radio Communications (PIMRC'93), Yokohama, Japan, pp. 468-472, Sep. 1993. MC-CDMA has been deemed to be a promising candidate for the downlink of fourth generation systems. Moreover, a MC/CDMA  
35 system with a variable spreading factor has been proposed as described in H. Atarashi and M. Sawahashi, "Variable Spreading Factor Orthogonal Frequency and Code Division

- 5 Multiplexing (VSF-OFCDM)", in 3<sup>rd</sup> International Workshop on Multi-Carrier Spread-Spectrum & Related Topics (MC-SS 2001), Oberpfaffenhofen, Germany, Sep. 2001.

For OFDM-based MIMO systems, one OFDM modulator is employed  
 10 on each transmitting point, while OFDM demodulation is performed independently for each receiving point. For OFDM, the signal stream is divided into  $N_c$  parallel sub-streams. The  $i^{\text{th}}$  sub-stream commonly termed  $i^{\text{th}}$  sub-carrier of the  $l^{\text{th}}$  symbol block (OFDM symbol) is denoted by  $X_{l,i}$ .  
 15 After serial to parallel conversion (S/P) performed by a S/P converter 701 an inverse discrete Fourier transform (DFT) with  $N_{\text{FFT}}$  points is performed by an IDFT transformer 703 on each block and, subsequently, the guard interval (GI) having  $N_{\text{GI}}$  samples is inserted by a GI block 705 to  
 20 obtain a signal  $x_{l,n}$  after parallel to serial (P/S) conversion performed by a P/S converter 703. After digital to analogue (D/A) conversion, the signal  $x(t)$  is transmitted over a mobile radio channel with an impulse response  $h(t, \tau)$ . The received signal at receive antenna  $v$   
 25 consists of superimposed signals from  $N_T$  transmitting points. Assuming perfect synchronisation, the received signal impinging at receive antenna  $v$  at sampling instants  $t = [n + 1]N_{\text{sym}} T_{\text{sp1}}$  is obtained

$$30 \quad y_{l,n}^{(v)} \triangleq y^{(v)}([n + 1]N_{\text{sym}} T_{\text{sp1}}) = \sum_{\mu=1}^{N_T} \int_{-\infty}^{\infty} h^{(\mu,v)}(t, \tau) \cdot x^{(\mu)}(t - \tau) d\tau + n(t) \Big|_{t=[n+1]N_{\text{sym}} T_{\text{sp1}}}$$

where  $n(t)$  represents additive white Gaussian noise, and  $N_{\text{sym}} = N_{\text{FFT}} + N_{\text{GI}}$  accounts for the number of samples per OFDM symbol. The  $*$  operator denotes convolution. The signal  $y_{l,n}$  received by the receiver is first serial to parallel  
 35 (S/P) converted by a S/P converter 709 and the guard interval is removed by a GI block 711. The information is

5 recovered by performing a discrete Fourier transform (DFT)  
 on the received block of signal samples (in Fig. 7 a FFT  
 transformer 713 is used) to obtain the output of the OFDM  
 demodulation  $Y_{1,i}$  in the frequency domain. The received  
 signal at receive antenna  $v$  after OFDM demodulation is  
 10 given by

$$Y_{1,i}^{(v)} = \sum_{\mu=1}^{N_T} X_{1,i}^{(\mu)} \cdot H_{1,i}^{(\mu,v)} + N_{1,i}$$

where  $X_{1,i}^{(\mu)}$  and  $H_{1,i}^{(\mu,v)}$  denotes the transmitted information  
 15 symbol and the channel transfer function (CTF) of transmit  
 antenna  $\mu$ , at sub-carrier  $i$  of the 1<sup>th</sup> OFDM symbol,  
 respectively. The term  $N_{1,i}$  accounts for additive white  
 Gaussian noise (AWGN) with zero mean and variance  $N_0$ .

20 When transmitting an OFDM signal over a multi-path fading  
 channel, the received signal will have unknown amplitude  
 and phase variations. For coherent transmission, these  
 amplitude and phase variations need to be estimated by a  
 channel estimator.

25 In the following, reference is made to pilot symbol-aided  
 channel estimation (PACE), where a sub-set of the  
 transmitted data is reserved for transmitting known  
 information, termed "pilot symbols". These pilots are used  
 30 as side information for channel estimation.

To formally describe the problem, the received pilot of  
 OFDM symbol  $1D_1$  at the  $(iD_2)^{\text{th}}$  sub-carrier

$$\begin{aligned}
 5 \quad Y_{\tilde{l}D_t, \tilde{l}D_f} &= \sum_{\mu=1}^{N_T} X_{\tilde{l}D_t, \tilde{l}D_f}^{(\mu)} H_{\tilde{l}D_t, \tilde{l}D_f}^{(\mu)} + N_{\tilde{l}D_t, \tilde{l}D_f} \quad \tilde{l} = \{1, 2, \dots, L/D_t\} \\
 &\quad \tilde{l} = \{1, 2, \dots, N_c/D_f\}
 \end{aligned}$$

where  $X_{\tilde{l}D_t, \tilde{l}D_f}^{(\mu)}$  and  $H_{\tilde{l}D_t, \tilde{l}D_f}^{(\mu, \nu)}$  denotes the transmitted pilot symbol and the channel transfer function (CTF) of transmit antenna  $\mu$ , at sub-carrier  $i = \tilde{l}D_f$  of the  $l = \tilde{l}D_t^{\text{th}}$  OFDM symbol, respectively. It is assumed that the CTF varies in the  $l$  and in the  $i$  variable, i.e. in time and in frequency. The term  $N_{\tilde{l}D_t, \tilde{l}D_f}$  accounts for additive white Gaussian noise.

Furthermore,  $l$  represents the number of OFDM symbols per frame,  $N_c$  is the number of sub-carriers per OFDM symbol,  $D_t$  and  $D_f$  denote the pilot spacing in frequency and time, and  $N_T$  is the number of transmit antennas. The goal is to estimate  $H_{l,i}^{(\mu)}$  for all  $\{l, i, \mu\}$  within the frame  $Y_{l,i}$  is measured. Additionally, the symbols  $X_{l,i}^{(\mu)}$  at the location  $(l, i) = (\tilde{l}D_t, \tilde{l}D_f)$  are known at the receiver. The channel estimation now includes several tasks:

1. The separation of  $N_T$  superimposed signals,
2. Interpolation in case that  $D_t$  or  $D_f$  are larger than one, and
- 25 3. Averaging over the noise  $N_{\tilde{l}D_t, \tilde{l}D_f}$  by means of exploiting the correlation of  $H_{\tilde{l}D_t, \tilde{l}D_f}^{(\mu, \nu)}$ .

In order to estimate  $H_{l,i}^{(\mu)}$  given  $Y_{\tilde{l}D_t, \tilde{l}D_f}$ , there are  $N_c$  equations with  $N_c N_T$  unknowns, when one OFDM symbol is considered. Thus, a straight-forward solution of this linear equation system does, in general, not exist. By

5 transforming  $Y_{\tilde{t}D, \tilde{t}D_f}$  to the time domain, the number of unknowns can be reduced, making it possible to solve the resulting equation system in the time domain. This approach has the advantage that DFT-based interpolation, which is a standard technique, can be combined with  
10 estimation and separation of  $N_T$  superimposed signals in one step, resulting in a computationally efficient estimator.

For time domain channel estimation for MIMO-OFDM systems, the received pilots of one OFDM symbol  $Y_{\tilde{t}D, \tilde{t}D_f}$  are pre-  
15 multiplied by the complex conjugate of the transmitted pilot sequence  $X_{\tilde{t}D, \tilde{t}D_f}^*$ , for  $1 \leq \tilde{t} \leq N'_p$ . Then the result is transformed into the time domain via an  $N'_p$ -point IDFT. Subsequently, the  $N_T$  superimposed signals are separated by a matrix inversion. The time domain channel estimate is  
20 obtained by filtering the output of the IDFT operation with a finite impulse response (FIR) filter. The DFT-based interpolation is performed simply by adding  $N_c - Q$  zeros for the channel impulse response (CIR) estimates, i.e. to extend the length of the estimate of length  $Q$  to  $N_c$   
25 samples. This technique is called of zero padding. An  $N'_p$ -point DFT transforms the CIR estimate of the pilots to the frequency response estimate of the entire OFDM symbol.

Estimators based on discrete Fourier transform (DFT) have  
30 the advantage that a computationally efficient transform in the form of the Fourier transform does exist and that DFT based interpolation is simple.

The performance of the estimation in general is dependent  
35 on the choice of the pilot symbols. It is desirable to choose a set of pilot sequences, which minimises the minimum



5 mean squared error (MMSE) criterium (which is a measure of  
the performance) and the computational complexity of the  
estimator. Estimators based on the least squares (LS) and  
the MMSE criterium for OFDM-MIMO systems have been  
systematically derived by Y. Gong and K. Letaief in: "Low  
10 Rank Channel Estimation for Space-Time Coded Wideband OFDM  
Systems," in Proc. IEEE Vehicular Technology Conference  
(VTC'2001-Fall), Atlantic City, USA, pp. 722-776, 2001.

I. Barhumil et al describe in: "Optimal training sequences  
15 for channel estimation in MIMO OFDM systems immobile  
wireless channels", International Zurich Seminar on  
Broadband Communications (IZS02), February, 2002 a channel  
estimation and tracking scheme for MIMO OFDM systems based  
on pilot tones. In particular, the authors describe a  
20 channel estimation scheme based on pilot tones being  
orthogonal and phase-shifted to each other. Although the  
pilot symbols described in the above-cited prior art allow  
an accurate channel estimation, an enormous computational  
complexity at the receiver is required in order to perform  
25 matrix inversions required by the channel estimation  
algorithm. Due to this high computational complexity, the  
estimation scheme described in the above prior art document  
cannot be implemented at low cost, so that the disclosed  
algorithm may not be suitable for mass-market mobile  
30 receivers.

Y. Li, et ("Simplified Channel Estimation for OFDM Systems  
with Multiple Transmit Antennas," IEEE Transactions on  
Wireless Communications, vol. 1, pp. 67-75, Jan. 2002),  
35 proposed a channel estimation scheme for OFDM with multiple  
transmit antennas which is based on the DFT transform. In  
particular, Li discloses a method for generating pilot

5 symbols to be transmitted by multiple transmit and receive antennas and to be exploited at the receiver for channel estimation. These pilot symbols are generated by multiplying a training sequence having good timing and frequency synchronisation properties by a complex sequence  
10 introducing an additional phase shift between the pilot symbols and between the subsequent values of each pilot symbol, as well. To be more specific, each value of a training sequence is multiplied by a complex factor, which introduces a phase shift, wherein the phase shift is  
15 dependent of a number being assigned to the value being multiplied, on a number assigned to the corresponding transmitting point and a total number of transmitting points. The pilot symbols are orthogonal and phase shifted to each other. The pilot symbols are modulated by an OFDM  
20 scheme and transmitted through a plurality of communication channels. At a receiver, which is one of a plurality of receivers, a signal being received includes a superposition of the plurality of transmitted signals through the plurality of communication channels. Li et al presented  
25 further a design rule for the pilot tones based on phase-shifted sequences which is optimum in the mean squared error (MSE) sense. Moreover, a matrix inversion, which is, in general, required for the estimator, can be avoided by choosing orthogonal pilot sequences. However, due to a  
30 difficulty of obtaining perfect orthogonality between training sequences, matrix inversions may be necessary.

Fig. 9 shows prior art channel estimation scheme as taught by Li, where the case of two transmitting antennas is  
35 considered.

5 The prior art channel estimator includes a plurality of multipliers, wherein Fig. 9 shows only three multipliers being associated with the  $k^{\text{th}}$  value of a  $n^{\text{th}}$  received sequence  $r[n,k]$ . A first multiplier 901, a second multiplier 903 and a third multiplier 905 arranged in parallel include first and second inputs and outputs, respectively. The output of the first multiplier 901 is connected to a first inverse fast Fourier transform (IFFT) block 907, the output of the second multiplier 903 is connected to a second IFFT block 909 and the output of the third multiplier 905 is connected to the third IFFT block 911. It should be mentioned here that in total,  $K$  multipliers are connected to each IFFT block, wherein  $K$  denotes a length of a received sequence in the frequency domain, and a total number of  $3K$  input signals are provided to the three IFFT blocks. Each of the IFFT blocks 907, 909 and 911 is operative to perform an inverse fast Fourier algorithm applied to  $K$  input values, respectively. Furthermore, each of the IFFT blocks 907, 909 and 911 includes a number of outputs, wherein only the first  $K_0$  outputs of each IFFT block are used. The respective remaining outputs are, for example, connected to ground.

$K_0$  outputs of the first IFFT block 907 are connected to a first estimation block 913 and the first  $K_0$  outputs of the third IFFT block 911 are connected to a second estimation block 915. The  $K_0$  outputs of the second IFFT block 909 are connected to the first estimation block 913 and to the second estimation block 915, respectively. The first estimation block 913 and the second estimation block 915 have  $K_0$  outputs, each of the outputs being connected to a corresponding filter 917 of a plurality of filters, each of the filters having an output, respectively. The  $K_0$  outputs

5 of the filters 917 corresponding to the first estimation block 913 are connected to a first Fourier transform (FFT) block 917 and the  $K_0$  outputs of the filter 917 corresponding to the second estimation block 915 are connected to a second FFT block 921. The first FFT block 919 and the second FFT block 921 have  $K$  outputs, where  $K$  is, as stated above, the number of sub-carriers. Furthermore, due to the simplified algorithm described by Li, the outputs of the first filters 917 corresponding to the first estimation block 913 are connected to the second estimation block 915 and the outputs of the filter 917 corresponding to the second estimation block 915 are further connected to the first estimation block 913, so that a plurality of feedback loops is established.

10 15 20 25 30 35

As stated above, Fig. 9 shows an example of the prior art estimator for the case of two transmit antennas, so that the received signal  $r[n,k]$  is a superposition of two transmitted signals being possibly corrupted by channel noise. The received signal is split into two received signals by a splitting means not shown in Fig. 9. The copies of the received signals are then multiplied by complex conjugated signals corresponding to the respective transmit antennas. Moreover, the pilot symbol transmitted by the first transmit antenna is multiplied by a complex conjugated version of the pilot symbol transmitted by the second antenna. More precisely, the  $K$  values of the first copy of the received signal are multiplied by  $K$  values of the complex conjugated version of the pilot symbol transmitted by the first antenna. The  $K$  values of the second version of the received signal is multiplied by  $K$  values of the complex conjugated version of the pilot symbol transmitted by the second transmit antenna.

5 Furthermore, the  $K$  values of the pilot symbol transmitted by the first antenna is multiplied by  $K$  complex conjugated values of the pilot symbol transmitted by the second transmit antenna in order to obtain intermediate values required by the subsequent channel estimation algorithm.

10

As stated above, all multiplications are performed in parallel, so that the  $K$  results from the multipliers 901 are fed to the first IFFT block 907.  $K$  results from the  $K$  multipliers 903 are fed to the second IFFT block 909.  $K$  results from the  $K$  multipliers 905 are fed to the third IFFT block 911. Each respective IFFT block is operative to perform an inverse fast Fourier transform in order to transform the frequency domain input signals into time domain output signals.

20

The first and the second estimation block, 913 and 915, are operative to perform a channel estimation algorithm based on the plurality of the input signals. More precisely, the first estimation block 913 receives  $3K_0$  input signals to generate  $K_0$  output signals corresponding to the channel impulse response of the first channel from the first transmit antenna to the considered receive antenna. The second estimation block 915 receives, in an analogue way,  $3K_0$  input signals to generate  $K_0$  output values corresponding to the second communication channel from the second transmit antenna to the receive antenna. The respective  $K_0$  output values are then filtered by filters 917.

35 As stated above, the respective output signals from the filters are fed back to the first and second channel estimation blocks 913 and 915, since the channel estimation

5 blocks 913 and 915 are operative to estimate the channel impulse response of the respective communication channels based on previously-calculated-values and on current values obtained from the IFFT blocks. Each estimation block applies an estimation algorithm where matrix by vector  
10 multiplications instead of matrix inversions are performed in order to calculate desired channel impulse responses. After filtering and zero padding to a length required by the following fast Fourier transform, a channel transfer function of the first and of the second communication  
15 channels are obtained.

As stated above, Li avoids matrix inversions by introducing an iterative scheme where matrix by vector multiplications appear and by exploiting the orthogonality of the pilot  
20 symbols. However, in order to calculate two channel impulse responses corresponding to the two communication channels, three inverse fast Fourier transforms, a splitting means and 3K multipliers are required. Moreover, the channel estimation algorithm applied by Li has still a  
25 high complexity due to the required matrix by vector multiplications. Hence, with an increasing number of transmit antennas, the complexity of the complicated estimation scheme proposed by Li rapidly increases due to the high number of complex valued multiplications. In  
30 addition, the multiplication of the two pilot symbols followed by an inverse Fourier transform is necessary in order to provide a plurality of intermediate values required for channel estimation. Hence, the estimation blocks 913 and 915 cannot operate independently, so that  
35 additional timing and control operations are necessary.

5 It is an object of the present invention to provide an improved concept for channel estimation with reduced complexity.

This object is achieved by an apparatus for estimating a  
10 plurality of channels in accordance with claim 1 or an apparatus for providing a plurality of different pilot sequences in accordance with claim 24 or an apparatus for providing a number of different pilot sequences in accordance with claim 25 or a method for estimating a  
15 plurality of channels in accordance with claim 26 or a method for providing a plurality of different pilot sequences in accordance with claim 27 or a method for providing a number of different pilot sequences in accordance with claim 28 or a method for providing a number  
20 of different pilot sequences in accordance with claim 29 computer programme in accordance with claim 30.

The present invention is based on the finding that a channel estimation based on orthogonal and phase-shifted  
25 pilot symbols with respect to each other can efficiently be performed by translating the phase shifts into delays, wherein an input signal including a superposition of a plurality of signals based on the pilot sequences transmitted through a plurality of communication channels  
30 is transformed into a transformed signal, so that the phase shifts between the plurality of pilot symbols are translated into delays. Hence, a set of discrete values of the transformed signals can be divided into a plurality of groups, each group having a delay with respect to the  
35 preceding groups, wherein each group represents channel information of a channel. In particular, it has been found that a single transformer can be applied for transforming

5 the phase shifts into delays, since the delayed groups actually include channel information, i.e. a channel impulse response of a communication channel, when a phase shift to delay transform is performed. Therefore, by exploiting the distinct delays in order to select the groups, the channel information can be obtained directly from the selected groups using only a single transformer.

For the sake of simplicity, in the following, only one receiving point being representative for the plurality of receiving points, will be discussed. However, it should be pointed out here that the following discussion and results can be applied to a plurality of receiving points in a straight-forward way. Furthermore, in the following an OFDM transmission system will be considered. However, the present invention can also be applied to channel estimation in single carrier modulation systems or in multichannel modulation techniques different from OFDM. To this end, preferably a guard interval is used so that the transmitted single carrier symbol is prevented from being affected by received signal from inter-symbol interference.

Referring again to the case of two transmitting points, an inventive apparatus for estimating a plurality of channels from a plurality of distinct transmitting points to a receiving point, derives an input signal from a signal received at the antenna of the receiving point. The input signal includes a superposition of a first signal based on a first pilot sequence transmittable from a first transmitting point and a second signal based on a second pilot sequence transmittable from a second transmitting point. The first pilot sequence and the second pilot sequence are orthogonal to each other within a



5 predetermined orthogonality range. If the first pilot  
sequence and the second pilot sequence are perfectly  
orthogonal to each other, then an inner product of these  
two sequences equals 0. However, since a perfect  
orthogonality is difficult to achieve, it is allowable that  
10 an absolute value of an inner product of the first pilot  
sequence and of the second pilot sequence is greater than  
or equal to 0 but preferably smaller than 0.2. Hence, the  
predetermined orthogonality range is defined by an interval  
having a first value equal to 0 and the last value equal to  
15 0.2.

If the first and the second pilot sequences have an  
additional phase shift to each other, then a transformer  
for transforming the input signal into a transformed signal  
20 translates the phase shifts into a delay, so that a first  
group of a set of discrete values of the transformed signal  
includes channel information of a first channel from the  
first transmitting point to the receiving point and a  
second group of the set of discrete values includes channel  
25 information of a second channel from the second  
transmitting point to the receiving point. Hence, as  
stated above, the first channel information is extracted  
simply by selecting the first group from the set of  
discrete values and the second channel information is  
30 extracted by selecting the second group from the set of  
discrete values. In order to obtain selected groups, the  
inventive apparatus further comprises a selector for  
selecting the first and the second group based on the delay  
between the first and the second group. Based on the  
35 selected groups, the channel information can be determined  
by a means for determining channel information.

5 In accordance with the present invention, an input signal is transformed by the transformer to translate the phase shift into a delay. Preferably, the transformer is operative to perform a Fourier transform, since a phase shift in the frequency domain is translated to a delay in  
10 the time domain by, for example, an inverse discrete Fourier transform and vice-versa. So if the pilot sequences are phase-shifted in the frequency domain, the resulting time domain signal after the inverse Fourier transform will be delayed. Furthermore, by assigning a  
15 certain phase shift to each pilot sequence, the corresponding delay in the time domain will be dependent on the transmit antenna. Provided that  $N_p \geq N_T Q$ , wherein  $N_p$  denotes a number of discrete values of the input signal, and by using appropriate sets of phase shifted sequences,  
20 the  $N_T$  superimposed signals can be simply separated by performing an inverse discrete Fourier transform.

While the estimator front and disclosed by Li et al requires pre-multiplications and a plurality of IDFT  
25 operations, only one IDFT operation is required to separate  $N_T$  superimposed signals by the inventive estimation scheme. The remaining part of the receiver will not be affected by this modification. Although certain phase-shifted sequences are perfectly suited in time-domain for OFDM  
30 channel estimation, other orthogonal sequences, such as sequences derived from Hadamard matrices, may be also be applied to the proposed simplified receiver structure, with some modifications resulting in a modest additional processing in time domain, which will be described later.

35

In general, a significant improvement of the proposed receiver structure compared to the prior art receiver

5 structure is the simplification of the estimator front-end. This simplification has no negative effects on the performance of the channel estimator. Moreover, if the phase shifted pilot sequences are appropriately designed, then the channel estimation scheme can further be  
10 simplified, since phase shifted pilot sequences are a perfect match to a Fourier transform in terms of separating the  $N_T$  superimposed signals without any substantial further processing.

15 In addition, an increasing number of transmitting points has only a slight impact on a complexity of the inventive channel estimation scheme, since irrespective of the number of transmitting points, only one transformer is required to transform the input signal into transformed signal so that  
20 the phase shifts are translated into delays. Accordingly, only one selector is applied to select the selected groups. This is a significant complexity reduction compared to the prior art discussed above, since the complexity of the prior art channel estimation scheme rapidly increases with  
25 an increasing number of transmitting points due to the required plurality of IDFT transformers in order to transform the plurality of (premultiplied) copies of the received signal and in order to obtain a further plurality of intermediate values required by the plurality of channel  
30 estimation blocks.

Furthermore, the inventive apparatus does not comprise any splitting means since only one input signal is directly transformed which leads to a further complexity reduction.  
35 Moreover, since only one transformer is used, an optional preprocessing of the input signal prior to transformation (windowing, zero padding etc.) is simpler.

5

Furthermore, due to the inventive channel estimation scheme, significantly less multiplications or no multiplications at all have to be performed which leads to a further significant complexity reduction when the input  
10 signal is not pre-multiplied by a plurality of complex conjugated pilot sequences. If the pilot sequences are pre-multiplied by a scrambling sequence in order to achieve better transmission characteristics of the signal to be transmitted, then only the values of one input signal have  
15 to be pre-multiplied for removing the influence of the scrambling sequence. If no pre multiplying is performed, then no multiplications prior to transforming are necessary. On the contrary, the prior art channel estimation scheme always requires a plurality of  
20 multiplications as described above.

Furthermore, the inventive channel estimation scheme is simplified since the transformed signal contains actually the channel information. Therefore, no matrix inversions or  
25 matrix by vector multiplications are necessary which further reduces the complexity.

Moreover, the inventive channel estimation scheme can be applied to any orthogonal sequences having different phase  
30 shifts to each other provided that these phase shifts are known at the transmitting point. Since these different phase shifts are transformed into delays, the inventive selector can always select proper groups from a plurality of delayed discrete values even when the discrete values  
35 belonging to a particular group are not succeeding each other.

5 Moreover, the performance of the proposed channel estimation scheme can be further increased by providing a plurality of different pilot sequences in accordance with a further embodiment of the present invention. In order to calculate an  $i^{\text{th}}$  value of a pilot sequence to be  
10 transmitted by a transmitting point from a number of transmitting points, the inventive apparatus for providing a plurality of different pilot sequences comprises a means for calculating a pilot sequence being operative to generate predetermined phase shifts between succeeding  
15 values of the pilot sequence to be transmitted and predetermined phase shifts between the pilot sequences as well.

To be more specific, the phase shifts between succeeding  
20 values of the pilot sequence to be transmitted are generated such that the phase shift between successive values of the pilot sequence is negative in a mathematical sense. Furthermore, the phase shift between the succeeding values depends on a number associated with the  
25 corresponding value in the pilot sequence.

In addition, in order to generate phase shifts between the plurality of pilot sequences, the phase shifts between succeeding values in a particular pilot sequence also  
30 depends on a number assigned to a transmitting point, the number being divided by a total number of transmitting points. Moreover, the generated pilot sequences are preferably scrambled by the same scrambling sequence, the length of the scrambling sequence being equal to the length  
35 of the pilot sequences, wherein each value of the pilot sequence to be generated is multiplied by a corresponding value of the scrambling sequence. Hence, all pilot

5 sequences include the same possibly complex valued scrambling sequence introducing an additional phase shift and amplitude modulation. Therefore, at the receiving point, the additional phase shift introduced by the scrambling sequence can be removed by applying a single  
10 multiplier by simply multiplying the input signal by a complex conjugated version of the scrambling sequence. Moreover, the inventive phase shift between each succeeding value of each pilot sequence is suited to an inverse discrete Fourier transform in order to translate the phase  
15 shifts into delays, since the inventive phase shift between succeeding values of each pilot sequence to be transmitted is negative in a mathematical sense and is hence a perfect counterpart of the IDFT (translating phase shifts into delays) since the IDFT introduces a phase shift in a  
20 positive mathematical sense. Hence, a simplified DFT based channel estimation scheme can be performed.

Moreover, in order to simplify the channel estimation scheme used at the receiving point, suitable orthogonal  
25 sequences can be used as pilot sequences (pilot symbols). In accordance with a further embodiment of the present invention, an apparatus for providing a number of different pilot sequences to be used for channel estimation comprises means for generating a Hadamard matrix having a number of  
30 columns, each column being orthogonal to the other columns, wherein the number of columns corresponds to the number of different pilot symbols. Based on the columns of the Hadamard matrix, the different pilot sequences can be calculated by, for example, a cyclic extension of each  
35 column of the Hadamard matrix, wherein each pilot sequence is derived from another column of the Hadamard matrix. Since the generated pilot sequences have a predetermined

5 phase shift to each other, these phase shifts translated.  
into delays at the receiver by, for example, applying an  
inverse discrete Fourier transform to obtain discrete  
values and to select groups containing channel information  
from the delayed discrete values. Moreover, this approach  
10 is suited for multi-carrier code division multiplex access  
transmission systems (MC-CDMA), where spreading in  
frequency direction is introduced in addition to the OFDM  
modulation. In order to introduce spreading in frequency  
direction, orthogonal signals based on columns of a  
15 Hadamard matrix can be applied, which simplifies a channel  
estimation procedure, since the same sequence can be  
applied for spreading in the frequency direction and for  
reduced complexity channel estimation. The inventive  
approach is also suited for channel estimation in multiple  
20 access transmission systems, like FDMA (frequency division  
multiple access) or TDMA (time division multiple access).

Further embodiments of the present invention are described  
in detail with respect to the following figures, in which:

25

Fig. 1 shows a block diagram of an inventive apparatus  
for estimating a plurality of channels;

30

Fig. 2 demonstrates a preferred transformation of an  
input signal into a plurality of delayed groups;

Fig. 3 shows a block diagram of an further inventive  
apparatus for providing a plurality of different  
pilot sequences;

35

5    Fig. 4    shows a block diagram of a inventive apparatus  
for providing a number of different pilot  
sequences;

10    Fig. 5    shows a block diagram of a further inventive  
apparatus for providing a number of different  
pilot sequences;

Fig. 6    shows a pilot grid structure;

15    Fig. 7    demonstrates an OFDM modulation and demodulation  
scheme; and

Fig. 8    shows a block diagram of prior art channel  
estimation schemes.

20

The apparatus shown in Fig. 1 comprises a multiplier 101  
having two inputs and one output. The output of the  
multiplier 101 is connected to a transformer 103 having a  
plurality of outputs for providing a transformed signal. The  
25    plurality of outputs of the transformer 103 is connected to  
a selector 105 having a control input 104 providing a delay  
information for proper group selection. The selector 105  
has a plurality of outputs, wherein a number of outputs is  
equal to a number of inputs of the selector 105 and, thus,  
30    equal to a number of outputs of the transformer 103. The  
plurality of outputs of the selector 105 is connected to a  
means 107 for determining channel information, the means  
107 having a plurality of outputs.

35    The apparatus shown in Fig. 1 demonstrates the inventive  
low complexity channel estimation scheme based on pilot  
signals being orthogonal to each other within the



5 predetermined orthogonality range and having a phase shift to each other. If the pilot sequences comprised of pilot symbols, each of the pilot sequences corresponding to one of a plurality of transmitting points, are scrambled by the same complex amplitude sequence, then the pilot sequences  
10 include a complex amplitude sequence and phase information. The transmitting points then transmit signals based on the pilot sequences through a plurality of communication channels, wherein prior to transmitting, the pilot sequences are modulated using, for example, an OFDM  
15 modulation scheme. A signal received at a receiving point (not shown in Fig. 1) includes a superposition of the plurality of transmitted signals and possibly a plurality of superimposed distortion signals representing channel noise. After a demodulation performed by applying an OFDM  
20 demodulation scheme, a received signal shown in Fig. 1 is obtained. The multiplier 101 is, hence, operative to multiply the received signal by a complex conjugated version of the amplitude sequence (scrambling sequence) in order to remove the amplitude information and phase shift  
25 introduced to each of the pilot sequences by scrambling. The received signal is a set of successive discrete received signal values and the multiplier 101 is operative to perform a single complex multiplication for each value of the set of successive discrete received signal values  
30 and a corresponding value of a set of successive discrete complex conjugated amplitude signal values, so that after a number of single complex multiplications, a set of successive discrete input values of an input signal is obtained.

35

The input signal includes a superposition of signals based on a plurality of pilot sequences, for example, based on a

5 first, a second and a third pilot sequence being  
transmitted from a first, a second and a third transmitting  
point. Hence, the input signal contains phase shifts of  
the pilot sequences, wherein the phase shifts are not  
removed by further pre-multiplications. Instead, the input  
10 signal is provided to the transformer 103 being operative  
to translate the phase shifts into delays.

The transformer 103 can be any transformer being able to  
translate phase shifts into delays. For example, the  
15 transformer 103 performs a Fourier transform or a fast  
Fourier transform or a discrete Fourier transform or an  
inverse Fourier transform or an inverse fast Fourier  
transform or an inverse discrete Fourier transform of the  
input signal. In particular, the input signal is a set of  
20 successive input signal values and the transformer is  
operative to transform the set of successive input signal  
values into the transformed signal, which is a set of  
discrete values, wherein a total number of discrete values  
of the set of discrete values of the transformed signal is  
25 equal to a total number of input signal values in the set  
of input signal values.

Hence, the transformer is operative to perform a single  
transform algorithm applied to the set of discrete values,  
30 wherein the transform algorithm can be, for example, one of  
the algorithms mentioned above applied to the total number  
of input signal values. The length of the input signal  
corresponds to a length of a training or pilot sequence  
multiplied by a total number of transmitting points.  
35 Hence, the length of the transformed signal is equal to the  
length of the input signal.

5 The selector 105 selects a number of groups, the number of groups being equal to the total number of transmitting points in order to obtain selected groups, wherein each group consists of an equal number of successive discrete values of the set of discrete values of the transformed  
10 signal. The selector is operative to select, as a group, a number of successive discrete values, wherein the number of successive discrete values is equal to the total number of discrete values of the transformed signal divided by the total number of transmitting points, wherein the total  
15 number of discrete values is obtained by the transformer.

For example, the selector is operative to select groups such that a first discrete value of the set of discrete values is a first discrete value in a first group at the  
20 output of the selector and a first discrete value of a second group of discrete values is a discrete value in the set of discrete values succeeding a discrete value having the highest order of the values selected to obtain the first group, wherein the first group and the second group  
25 have corresponding distinct delays, the delays being obtained by the transformer. If the input signal includes, in a superimposed manner, a third signal based on a third pilot sequence transmittable from a third transmitting point, the transformer translates a further phase shift of  
30 the third group into a further delay, so that a third group of the set of discrete values includes channel information of a third channel from the third transmitting point to the receiving point and the selector selects the third group from the set of discrete values to obtain a selected third  
35 group having a further delay associated with the third group. Hence, if the input signal includes a plurality of superimposed signals corresponding to a plurality of

5 transmitting points, the selector 105 selects a further group of the plurality of groups on the basis of a delay corresponding to the further group as depicted in Fig. 1.

The groups being selected by the selector based on a delay  
10 information via the control input 104 or based on a fixed setting (no control input is required in this case) are provided to the means 107 for determining channel information based on the selected groups. If the pilot symbols are orthogonal to each other within the  
15 orthogonality range and if the pilot symbols have a predetermined phase shift with respect to each other, then each of the selected groups contains channel information corresponding to a particular channel from a particular transmitting point to the receiving point. In this case,  
20 the means 107 is operative to receive the selected groups and to output the selected groups, since each of the groups includes channel information of the particular channel, as will be shown later. In order to output the selected groups, the means 107 can be designed in such a way that  
25 the inputs of the means 107 are directly connected to the outputs of the means 107. If there is no channel noise or if the channel noise is negligible, then the means 107 for determining channel information outputs the selected groups, each group including, for example, a channel  
30 impulse response of a particular channel as channel information. Furthermore, the means 107 can include a time frequency conversion means, for example, a DFT based transformer for obtaining a channel transfer function by transforming the determined channel impulse response of a  
35 particular channel into the frequency domain in order to obtain the channel transfer function as the channel information.

5

Depending on pilot sequences applied to channel estimation, a group of the selected groups and a further group of the selected groups may include channel information of a channel and channel information of a further channel in a superimposed manner. Furthermore, depending on the design of pilot sequences, a group of the selected groups may include a superposition of the channel information of a channel being multiplied by a phase shift factor and of a further channel information of a further channel being multiplied by a further phase shift factor, wherein a further group of the selected groups may include a superposition of the channel information of the channel being multiplied by the complex conjugated phase shift factor and of the further channel information of the further channel being multiplied by the complex conjugated further phase shift factor, wherein the phase shift factor and the further shift factor are caused by the design of the pilot sequences. In this case, the means 107 is operative to determine the channel information of the channel and the further channel information of the further channel using the group and the further group by, for example, solving a set of linear equations and removing the additional phase shift factors. For example, the means 107 applies phase shift operations and additions and/or subtractions to the group and to the further group in order to determine channel information. If, for example, pilot sequences based on columns of a Hadamard matrix are applied to channel estimation, then the phase shift factor is a function of a phase shift of  $180^\circ$  divided by the total number of transmitting points. Using this information, the known phase shifts are removed to determine the channel information.

5

If the channel noise cannot be neglected, then the channel information in the selected\_groups is affected by a distortion signal related to channel noise. In order to suppress the distortion signal, the means 107 may comprise an estimator being operative to estimate the channel information from the corrupted channel information by, for example, applying a minimum mean squared error (MMSE) estimator, a least squares (LS) estimator, a maximum-likelihood (ML) estimator or a maximum a posteriori (MAP) estimator (being a particular embodiment of a ML estimator). If the MMSE estimator is applied to estimate channel information, then the estimator performs filtering of the corrupted channel information, wherein the filter has filter coefficients, wherein each filter coefficient is determinable from a multiplication of a first matrix by a second matrix, wherein the first matrix is a cross-correlation (in general: cross-covariance) matrix between channel information and corrupted channel information and the second matrix is an inverse of an autocorrelation (in general: auto-covariance) matrix of the corrupted channel information.

The pilot sequences applied to channel estimation in an OFDM transmission system are commonly used to modulate discrete carriers in a multi-carrier modulation scheme at a predetermined time instant corresponding to the time instant at which pilot sequences are to be transmitted. Hence, the inventive apparatus may further comprise a controller for detecting the input signal in a received signal and for enabling the transformer, the selector or the means for detecting only when the input signal

35

5 including pilot sequences is detected in the received signal.

Alternatively, the pilot sequences can be used to modulate the same pilot carrier in a multi-carrier modulation scheme  
10 in order to estimate time varying coefficients of a channel transfer function of a communication channel, wherein the coefficients of the channel transfer function are determined by the pilot carrier. Hence, the inventive apparatus can comprise a controller for detecting the pilot  
15 carrier in a received signal, including successive multi-carrier modulated symbols and for collecting values of the pilot carrier at time instants corresponding to the transmitting instants to obtain the input signal, wherein the channel information obtained by processing the input  
20 signal using the transformer selector and the means for detecting includes a behaviour of a multi-carrier channel from transmitting points to receiving points defined by the pilot carrier over time. The channel information including the behaviour of the multi-carrier channels is, for  
25 example, related to a velocity of a mobile receiver causing, for example, a Doppler shift related to the relative velocity between transmitter and receiver. In order to estimate the Doppler shift, changes of a coefficient of the channel transfer function over time can  
30 be exploited.

If the pilot sequences are transmitted at distinct time instances and are not succeeding each other, preferably an interpolation is performed in order to obtain intermediate  
35 values of channel information between time instances corresponding to the time instants at which pilot sequences are transmitted. Hence, the means for determining channel

5 information may comprise a further means for interpolation being operative to interpolate between a first channel information obtained at a first time instant and a second channel information obtained at a second time instance, wherein the intermediate interpolated channel information  
10 can, for example, be determined by applying a well known Wiener interpolation technique (Wiener filter) based on the first and the second channel information or, for example, by applying a Lagrange interpolation scheme.

15 Fig. 2 demonstrates a principle of exploiting the DFT properties by using phase-shifted sequences in the frequency domain, wherein the DFT algorithm separates  $N_T$  signals in the time domain, wherein  $N_T$  corresponds to a number of transmitting points. The frequency domain input  
20 signal can include pilots having a spacing in frequency denoted by  $D_F$ , as depicted in Fig. 2. The pilots are orthogonal to each other within the orthogonality range and have different phase shifts which can be translated into delays by applying the DFT-based transform yielding a time  
25 domain transformed signal. The transformed signal in the time domain includes  $N_T$  groups including channel information like, for example, a channel impulse response of a particular communication channel. Each of the groups includes  $N_p/N_T$  discrete values, wherein  $N_p$  denotes a total  
30 length of the input signal. The groups transformed by the transformer are time-delayed, wherein a second group has a delay with respect to a first group, so that the discrete values of the second group do not overlap with the discrete values of the first group. Accordingly, the  $N_T^{\text{th}}$  group  
35 corresponding to the  $N_T$  transmitting point has the same delay with respect to a preceding group.  $N_{\text{FFT}}$  denotes a



5 number of discrete FFT points being dependent on the pilot spacing in frequency domain.

It is well known that a very efficient implementation of the DFT is the fast Fourier transform (FFT) algorithm. For  
10 optimum efficiency, the number of points of the FFT should be a power of 2. It is important to note that the interpolation ratio should be  $D_f$ .

Fig. 3 shows a conceptual block diagram of an inventive  
15 apparatus for estimating a plurality of channels from a plurality of distinct transmitting points to a receiving point.

The apparatus shown in Fig. 3 comprises a frequency domain  
20 (FD) window 301 having  $N_p$  inputs corresponding to  $N_p$  discrete values of an input signal provided to the frequency window 301 and  $N_p$  outputs connected to a  $N_p$ -IFFT transformer 303. The IFFT transformer 303 has  $N_p$  outputs connected to a selector 305. The selector 305 has a  
25 plurality of outputs, wherein each succeeding group of  $Q$  outputs is connected to a corresponding filter and/or threshold means 307. Each of the filter means 307 has  $Q$  outputs connected to a corresponding zero padding means 309, wherein each of the zero padding means 309 has  $N_c$   
30 outputs connected to a corresponding  $N_c$ -point FFT transformer 311 of a plurality of FFT transformers. Each of the FFT transformer 311 has  $N_c$  outputs connected to a corresponding inverse window means 313, each of the inverse window means 313 having  $N_c$  outputs. The plurality of the  
35 filter means 307, the plurality of the zero padding means 309, the plurality of the FFT means 311 and the plurality of the inverse window means 313 are part of a means 315 for

5 determining channel information of the plurality of channels based on the selected groups in accordance with a further embodiment of the present invention.

The  $N_p$  discrete values of the input signal are first  
10 windowed by the frequency domain window means 301 in order to avoid leakage affects which can be caused by the following IFFT transformation performed by the IFFT transformer 303. The inventive apparatus comprises single means 301 for windowing the input signal to obtain a  
15 windowed input signal to be used as the input signal for the transformer. The input signal includes a plurality of pilot sequences having different phase shifts with respect to each other, wherein each of the pilot sequences corresponds to a transmitting point, transmitting the pilot  
20 sequence for channel estimation.

The IFFT transformer 303 translates the phase shifts into delays by performing an IFFT transform applied to the  $N_p$  values of the input signal in order to obtain a transformed  
25 signal. It is to be remarked here that the IFFT transformer 303 performs a single IFFT algorithm applied to the input signal. Hence, the transformed signal consists of successive  $N_p$  discrete values being related to the delays.

30

The selector 305 selects a plurality of groups from a set of discrete values of the transformed signal, wherein each selected group of the selected groups actually includes channel information in the form of a channel impulse  
35 response of each communication channel.

5 Due to a possible channel noise, the channel information is corrupted by a distortion signal related to the channel noise. Hence, the selected groups are filtered by the respective filter means 307 in order to estimate the channel information from the corrupted channel information.

10 The filter means 307 can be operative to perform a detection of the channel information from the noisy channel information. This can be performed by applying a minimum mean squared estimation by filtering the selected groups, wherein each filter means 307 comprises a filter having

15 filter coefficients, wherein each filter coefficient can be determined from a multiplication of a first matrix by a second matrix, the first matrix being a cross-correlation matrix between channel information and the corrupted channel information and the second matrix being an inverse

20 of an auto-correlation matrix of the corrupted channel information as described above. Alternatively, a simple threshold operation can be performed to estimate the channel information by means of hard detection. Hence, the filter means 307 outputs a plurality of channel impulse

25 responses as channel information corresponding to each communication channel. In order to obtain a channel transfer function of a particular channel impulse response, the means 315 for determining channel information comprises means for transforming the channel impulse responses into

30 frequency domain.

In its basic form, DFT based interpolation is performed simply by adding  $N_c - Q$  zeros to the channel impulse response estimate, thus extending the length of each

35 channel impulse response to  $N_c$  samples by means of zero padding by for example attaching the  $N_c - Q$  zeros at the end of each channel impulse response. Hence, after zero padding

5 performed by the respective zero padding means 309, a length of each channel impulse response is extended to a total length of  $N_c$ . In the next step, the extended channel impulse responses in the time domain are transformed into frequency domain by applying for example a fast Fourier transform to each extended channel impulse response by the  
 10 FFT means 311. In order to obtain a channel transfer function corresponding to each channel impulse response, an inverse window operation is performed in order to remove the windowing effects caused by the frequency domain window  
 15 means 301.

Fig. 4 shows a conceptual block diagram of an inventive apparatus for providing a plurality of different pilot sequences to be used for channel estimation.

20 The apparatus shown in Fig. 4 comprises means 401 calculating an  $i^{\text{th}}$  value of a pilot sequence to be transmitted by a  $\mu^{\text{th}}$  transmitting point of  $N_T$  transmitting points.

25 In order to calculate distinct pilot sequences the means 401 uses the following equation for calculating an  $i^{\text{th}}$  value  $X_i^{(\mu)}$ :

$$30 \quad X_i^{(\mu)} = e^{-j2\pi(i-1)(\mu-1)/N_T} X_i^{(s)}$$

wherein  $N_T$  denotes a number of transmitting points being greater than or equal to 3 and wherein  $X_i^{(s)}$  denotes an  $i^{\text{th}}$  value of a scrambling sequence, wherein a length of the scrambling sequence is equal to a length of the pilot  
 35 sequence.

5 Hence, the pilot sequence corresponding to a first transmitting point, wherein  $\mu=1$ , is identical to the scrambling sequence. A  $n^{\text{th}}$  pilot sequence  $\mu=n$  to be transmitted by an  $n^{\text{th}}$  transmitting point comprises a number of discrete values related to the phase shifts of the  $n^{\text{th}}$   
10 pilot sequence, wherein each value of the  $n^{\text{th}}$  pilot sequence is multiplied by the scrambling sequence. The phase shifts of each value of the pilot sequence depend on a number of the value being calculated, wherein the number of the value is associated with a position of the value within the pilot sequence. Furthermore, the phase shift of  
15 the  $n^{\text{th}}$  pilot sequence with respect to the other pilot sequence depends on a number of transmitting points divided by a total number of transmitting points  $N_T$ . Hence, succeeding values of each pilot sequence have a phase shift with respect to each other, wherein the phase shift is  
20 negative in a mathematical sense, due to a negative sign appearing in the exponent of the exponential function.

Hence, the pilot sequences provided by the inventive  
25 apparatus are suited for low complexity DFT based channel estimation. By using the inventive phase shifted pilot sequences, the properties of the Fourier transform can efficiently be exploited to separate the  $N_T$  superimposed signals. It is well known that a phase shifted signal in  
30 the frequency domain is translated to a delay in the time domain by the Fourier transform and vice versa. So, by using phase shifted pilot sequences in the frequency domain, the resulting time domain signal will be delayed. Furthermore, by assigning a certain phase shift as  
35 described above to each transmit antenna's pilot, the corresponding delay in the time domain will be dependent on the transmit antenna. Provided that a length of each

5 training sequence is greater than or equal to  $N_T Q$ , where  $Q$  denotes a length of a channel having a maximum length of the plurality of the communication channels to be estimated, the  $N_T$  superimposed signals can be separated completely simply by performing an inverse discrete Fourier  
10 transform.

It has been discussed above that phase shifted pilot sequences provided by the inventive apparatus shown in Fig. 4 are suited to time domain MIMO OFDM channel estimation  
15 since these sequences are the perfect match to the IDFT operation. Nevertheless, other orthogonal sequences may also be applied to a low complexity channel estimation with some additional processing in time domain.

20 Fig. 5 shows a conceptual block diagram of a further inventive apparatus for providing a number of different pilot sequences to be used for channel estimation, wherein the pilot sequences are orthogonal sequences based on columns of a Hadamard matrix.

25 The apparatus shown in Fig. 5 comprises a means 501 for generating a Hadamard matrix having a number of columns, wherein the number of columns corresponds to the number of different pilot sequences (pilot symbols). The means 501  
30 has a number of outputs, the number of outputs being equal to the number of columns of the Hadamard matrix. The outputs of the means 501 are connected to a means 503 for calculating different pilot sequences. The means 503 for calculating different pilot sequences has a number of  
35 outputs for providing the different pilot sequences.

5 The means 501 for generating a Hadamard matrix calculates columns of the Hadamard matrix being orthogonal to each other. The number of columns of the Hadamard matrix is provided to the means 503 for calculating different pilot sequences, wherein the means 503 calculates the different  
10 pilot sequences on the basis of the columns of the Hadamard matrix. Each pilot sequence is derived from another column of the Hadamard matrix. In order to generate a pilot sequence, the corresponding column of basis functions given by the columns of the Hadamard matrix can for example be  
15 periodically extended to a pilot sequence length.

However, the inventive pilot sequences based on Hadamard codes cannot be applied to the simplified receiver structure discussed above in a straight forward way for a  
20 number of transmitting points being greater than 2. With some additional processing a channel estimation scheme based on Hadamard codes can be simplified. For example, if four transmitting points are applied to transmit pilot sequences, then a channel information determined by a DFT  
25 based channel estimation scheme has an additional phase shift factor which is a function of a phase shift of 180 degrees divided by four. Hence, the additional processing necessary to determine channel information is small since only phase shift operations, additions and subtractions are  
30 required in order to solve a set of linear equations.

If, for example, eight transmitting points are applied to transmit pilot sequences, the estimated channel information has an additional phase shift factor which is a function of  
35 a phase shift by 180 degrees divided by the total number of transmitting points which is eight in this case. Hence, only four phase shifting and four add and subtract

5 operations are necessary. Note that application to Walsh sequences is straight forward since Walsh sequences are obtained by rearranging the columns of the Hadamard matrix, i.e. assigning different pilot sequences to the transmit antennas.

10

Pilot aided channel estimation (PACE) was first introduced for single carrier systems and required a flat fading channel, as described by J.K. Cavers, "An Analysis of Pilot Symbol Assisted Modulation for Rayleigh Fading Channels,"  
15 IEEE Transactions on Vehicular Technology, vol. VT-40, pp. 686-693, Nov. 1991. It is based on periodically inserting known symbols, termed pilot symbols in the data sequence. If the spacing of the pilots is sufficiently close to satisfy the sampling theorem, the channel estimation and  
20 interpolation for the entire data sequence is possible. When extending the idea of PACE to multi-carrier systems, it must be taken into account that for OFDM fading fluctuations in two dimensions occur, i.e., in time and frequency. In order to satisfy the two-dimensional sampling  
25 theorem, the pilot symbols are scattered throughout the time/frequency grid, which yields to a two-dimensional pilot grid.

Possible realizations of pilot grid structures for OFDM  
30 channel estimation are illustrated in Fig. 6. One possibility to structure a pilot grid is to transmit one OFDM symbol containing only pilots followed by  $D_t-1$  data symbols. This sequence is shown in the left diagram in Fig. 6. This scheme is applicable for channels with little time  
35 variations, as observed in an indoor environment. In this case, no interpolation (in frequency direction) is necessary. Another possibility is to transmit the pilots on



5 reserved carriers as shown in the middle diagram in Fig. 6. This scheme can support mobility but requires interpolation in frequency direction. A more efficient solution is to employ a scattered pilot grid, as shown in the right diagram in Fig. 6. The structure for OFDM signalling allows  
10 a channel estimator to use both time and frequency correlations. With such a scattered pilot grid, the property of OFDM, that adjacent sub-carriers as well as adjacent symbols are correlated, can be exploited for channel estimation. Thus, the overhead due to pilots can be  
15 reduced but interpolation in time and frequency is required.

For pilot symbol aided channel estimation (PACE) based on a scattered pilot grid, known pilot symbols are multiplexed  
20 into the data stream. Interpolation is used to obtain the channel estimate for the information carrying symbols. PACE for single carrier systems was introduced by Cavers in the above mentioned prior art document. P. Hoeher, S. Kaiser, and P. Robertson, "Two-Dimensional Pilot-Symbol-Aided  
25 Channel Estimation by Wiener Filtering", in Proc. IEEE Intern. Conf. On Acoustics, Speech, and Signal Processing. (ICASSP'97), Munich, Germany pp. 1845-1848, 1997, and R. Nilsson, O. Edfors, M. Sandell, and P. Börjesson, "An Analysis of Two-Dimensional Pilot-Symbol Assisted  
30 Modulation for OFDM", in Proc. IEEE Intern. Conf. On Personal Wireless Communications (ICPWC'97), Mumbai (Bombay), India, pp. 71-74, 1997. They propose two-dimensional 2D filtering algorithms for PACE. Such a 2D estimator structure is generally too complex for practical  
35 implementation. To reduce the complexity, separating the use of time and frequency correlation has been proposed. This combined scheme, termed double 1-dimensional PACE uses

5 separate Wiener filters, one in frequency direction and one in time direction.

A general formal description of a regular grid in a 2D plane can be found in Y. Li, "Pilot-Symbol-Aided Channel  
10 Estimation for OFDM in Wireless Systems", IEEE Transactions on Vehicular Technology, vol. 49, pp. 1207-1215, July 2000.

The total number of pilots transmitted by one frame is depicted as  $N'_p = N_c / D_f$  and  $N''_p = L / D_t$ , representing the  
15 number of pilots in frequency and time direction, respectively. The following notation will be used. Given a variable describing a 2D structure X, the subsets which describe the dimension corresponding to frequency and time directions are denoted by X' and X'', respectively. As a  
20 general convention, variables describing pilot symbols will be marked with a "~" in the following

For MIMO systems every transmit antenna signal uses its own pilot, to enable the receiver to separate the superimposed  
25 signals. To describe pilot symbol assisted channel estimation, it is useful to define a subset of the received signal sequence containing only pilots,  $\{\tilde{X}_{l,\tilde{t}}^{(\mu)}\} = \{X_{l,i}^{(\mu)}\}$  with  $l = \tilde{l}D_f$  and  $i = \tilde{t}D_t$ . So, the pilot sequences transmitted at  $D_f$  times lower rate  $\tilde{l} = \lfloor l / D_f \rfloor$  in frequency direction, and a  $D_t$   
30 times lower rate  $\tilde{t} = \lfloor t / D_t \rfloor$  in time direction, respectively. It is assumed that the pilots  $\{\tilde{X}_{l,\tilde{t}}^{(\mu)}\}$  are chosen from a phase shift keying (PSK) constellation  $|\tilde{X}_{l,\tilde{t}}^{(\mu)}| = 1$ . Before transmission, the pilots  $\{\tilde{X}_{l,\tilde{t}}^{(\mu)}\}$  are multiplied by an outer

- 5 pilot sequence  $\{\tilde{X}_{0_{T,j}}\}$  which is identical for all transmit antennas to yield the transmitted pilot sequence.

$$\tilde{X}_{T,j}^{(\mu)} = \tilde{X}_{0_{T,j}} \cdot \tilde{X}_{T,j}^{(\mu)}$$

- 10 The outer pilot sequence  $\{\tilde{X}_{0_{T,j}}\}$  is chosen to have a low peak to average power ratio (PAPR) in the time domain and/or to have good correlation properties for synchronisation etc. In any case, the outer pilot sequence is introduced solely for the sake of completeness.

15

- At the receiver, the cyclic prefix is removed and an FFT is performed to yield the received signal after OFDM demodulation. Assuming perfect synchronisation, the received signal  $Y_{l,i}$  is obtained. For channel estimation,
- 20 the received signals at the pilot positions are demultiplexed from the data stream, and after removing the outer pilot sequence, by dividing through  $\tilde{X}_{0_{T,j}}$  the received pilot is obtained.

$$25 \quad \tilde{Y}_{T,j} \stackrel{\Delta}{=} Y_{l,i \in G} = \sum_{\mu=1}^{N_T} X_{l,i \in G}^{(\mu)} H_{l,i \in G}^{(\mu)} + N_{l,i \in G}$$

where G is the subset of the OFDM frame containing the pilots.

- 30 Considering the pilot sequence of OFDM symbol  $l = \tilde{l}D_t$  from transmit antenna  $\mu$  which can be expressed by a column size factor of size  $N_p'$

$$\begin{aligned}
\tilde{Y}_T^t &= \sum_{\mu=1}^{N_T} \tilde{X}_T^{t(\mu)} \tilde{H}_T^{t(\mu)} + \tilde{N}_T^t & \in \mathbb{C}^{N_p' \times 1} \\
&= \sum_{\mu=1}^{N_T} \tilde{X}_T^{t(\mu)} \tilde{F} I_{N_p \times Q} \tilde{h}_T^{t(\mu)} + \tilde{N}_T^t
\end{aligned}$$

where the transmitted pilot sequence, the channel transfer function (CTS) and additive noise term are given by

$$\begin{aligned}
\tilde{X}_T^{t(\mu)} &= \text{diag}(\tilde{X}_{T,1}^{t(\mu)}, \dots, \tilde{X}_{T,N_p'}^{t(\mu)}) \in \mathbb{C}^{N_p' \times N_p'} \\
\tilde{H}_T^{t(\mu)} &= [\tilde{H}_{T,1}^{t(\mu)}, \dots, \tilde{H}_{T,N_p'}^{t(\mu)}]^T \in \mathbb{C}^{N_p' \times 1} \\
\tilde{h}_T^{t(\mu)} &= [\tilde{h}_{T,1}^{t(\mu)}, \dots, \tilde{h}_{T,Q}^{t(\mu)}]^T \in \mathbb{C}^{Q \times 1} \\
\tilde{N}_T^t &= [\tilde{N}_{T,1}^t, \dots, \tilde{N}_{T,N_p'}^t]^T \in \mathbb{C}^{N_p' \times 1}
\end{aligned}$$

the  $N_p' \times N_p'$  DFT-matrix  $\tilde{F}$  transforms the CIR into the frequency domain, defined by

$$\{\tilde{F}\}_{i+1,n+1} = e^{-j2\pi i n / N_p'}; \quad 0 \leq i \leq N_p' - 1, \quad 0 \leq n \leq N_p' - 1$$

In case that  $Q < N_p'$ , the last  $N_p' - Q$  of the DFT output need to be removed, which can be formally performed by the matrix  $I_{N_p' \times Q} = [I_{Q \times Q}, 0_{N_p' - Q \times Q}]^T$  of dimension  $N_p' \times Q$ , with entries equal to 1 at the main diagonal and 0 elsewhere. For  $Q = N_p'$ , the matrix  $I_{N_p' \times N_p'}$  becomes the identity matrix. In practice, the DFT transformation can be efficiently generated using a  $N_p'$ -point FFT. In case that  $Q < N_p'$ , the last  $N_p' - Q$  outputs are skipped.

5

Hence, the flowing equation follows

$$\tilde{Y}'_l = \tilde{X}'_l \tilde{H}'_l + \tilde{N}'_l = \tilde{X}'_l \tilde{F}_{N_T} \tilde{h}'_l + \tilde{N}'_l$$

10 where

$$\begin{aligned}\tilde{X}'_l &= [\tilde{X}'^{(1)}_l, \dots, \tilde{X}'^{(N_T)}_l] \in \mathbb{C}^{N'_p \times N_T N'_p} \\ \tilde{H}'_l &= [\tilde{H}^{(1)}_l, \dots, \tilde{H}^{(N_T)}_l]^T \in \mathbb{C}^{N_T N'_p \times 1} \\ \tilde{h}'_l &= [\tilde{h}^{(1)}_l, \dots, \tilde{h}^{(N_T)}_l]^T \in \mathbb{C}^{N_T Q \times 1} \\ \tilde{F}_{N_T} &= \text{diag}(\tilde{F}I_{N'_p \times Q}, \dots, \tilde{F}I_{N'_p \times Q}) \in \mathbb{C}^{N_T N'_p \times N_T Q}\end{aligned}$$

15

Referring now to a design of phase shifted pilot sequences,  
20 the set of  $N_T$  phase shifted pilot sequences of length  $N'_p$   
is defined by

$$\tilde{X}'_{l,\tilde{l}}^{(\mu)} = e^{-j2\pi(\tilde{l}-1)(\mu-1)/N_T}; \quad \mu = \{1, \dots, N_T\}, \quad \tilde{l} = \{1, \dots, N'_p\}$$

25 wherein the pilot sequences defined by the above equation  
are in accordance with the preferred embodiment according  
to the present invention.

In stead of pre-multiplying the received signal prior to  
30 the IDFT operation, the received pilot signal of OFDM  
symbol  $l = \tilde{l}D_f$ ,  $\tilde{Y}'_l$  is directly transformed into the time  
domain:

5

$$\zeta_{\tilde{T}} \stackrel{\Delta}{=} \frac{1}{N'_p} \tilde{F}^H \tilde{Y}'_{\tilde{T}} = \frac{1}{N'_p} \sum_{\mu=1}^{N_T} \tilde{F}^H \tilde{X}_{\tilde{T}}^{(\mu)} \tilde{F} I_{N'_p \times Q} \tilde{h}_{\tilde{T}}^{(\mu)} + \frac{1}{N'_p} \tilde{F}^H \tilde{N}'_{\tilde{T}} \quad \in \mathbb{C}^{N'_p \times 1}$$

Hence, only one IDFT is required to generate  $\zeta_{\tilde{T}}$

10 As to the properties of the DFT, phase shifted sequences are transformed by the DFT to a time shift. By assigning each transmit antenna its own phase shift, the time domain signal  $\zeta_{\tilde{T}}$  is separated perfectly if  $Q \leq N'_p / N_T$ .

15 In order to analyse the following equation, it is useful to examine the components of the vector  $\zeta_{\tilde{T}}$  appearing in the above equation. The  $n^{\text{th}}$  entry of  $\zeta_{\tilde{T}}$  is in the form

20

$$\begin{aligned} \zeta_{\tilde{T},n} &\stackrel{\Delta}{=} \frac{1}{N'_p} \sum_{\tilde{T}=1}^{N'_p} \tilde{Y}_{\tilde{T},\tilde{T}} e^{j2\pi \cdot (\tilde{T}-1) \cdot (n-1) / N'_p} & n = \{1, \dots, N'_p\} \\ &= \frac{1}{N'_p} \sum_{\tilde{T}=1}^{N_p} \sum_{\mu=1}^{N_T} \tilde{X}_{\tilde{T},\tilde{T}}^{(\mu)} e^{j2\pi \cdot (\tilde{T}-1) \cdot (n-1) / N'_p} \sum_{q=1}^Q \tilde{h}_{\tilde{T},q}^{(\mu)} e^{-j2\pi \cdot (\tilde{T}-1) \cdot (q-1) / N'_p} \\ &\quad + \frac{1}{N'_p} \sum_{\tilde{T}=1}^{N'_p} \tilde{N}_{\tilde{T},\tilde{T}} e^{j2\pi \cdot (\tilde{T}-1) \cdot (n-1) / N'_p} \\ &= \frac{1}{N'_p} \sum_{\mu=1}^{N_T} \sum_{q=1}^Q \tilde{h}_{\tilde{T},q}^{(\mu)} \sum_{\tilde{T}=1}^{N'_p} \tilde{X}_{\tilde{T},\tilde{T}}^{(\mu)} e^{j2\pi \cdot (\tilde{T}-1) \cdot (n-q) / N'_p} + \tilde{n}_{\tilde{T},n} \\ &= \frac{1}{N'_p} \sum_{\mu=1}^{N_T} \sum_{q=1}^Q \tilde{h}_{\tilde{T},q}^{(\mu)} F_{N'_p} \left( \tilde{X}_{\tilde{T},\tilde{T}}^{(\mu)} \right)_{q-n} + \tilde{n}_{\tilde{T},n} \end{aligned}$$

25

- 5 Where  $\tilde{n}_{I,n}$  is the IDFT of  $\tilde{N}_{I,I}$ . Hence, calculation of the DFT of the phase shifted pilot sequences in accordance with the preferred embodiment of the present invention leads to

$$F_{N'_p}(\tilde{X}_{I,I}^{(\mu)})_{q-n} = N'_p f_{N'_p}(n-q-(\mu-1)N'_p/N_T) = N'_p \delta_{n-q-(\mu-1)N'_p/N_T}.$$

10

It is noted that this is identical to the DFT of  $\tilde{X}_{I,I}^{(0)} * \tilde{X}_{I,I}^{(\mu)}$  since  $\tilde{X}_{I,I}^{(0)}$  is the all one sequence. Hence, the desired result for  $\zeta_{I,n}^{(\mu)}$  is obtained by

15

$$\begin{aligned} \zeta_{I,n} &= \sum_{\mu=1}^{N_T} \sum_{q=1}^Q \tilde{h}_{I,q}^{(\mu)} \delta_{n-q-(\mu-1)N'_p/N_T} + \tilde{n}_{I,n} \\ &= \tilde{h}_{I,n}^{(\mu)} + \tilde{n}_{I,n} \quad \text{with } n = q + (\mu-1)N'_p/N_T \quad \text{and } Q \leq N'_p/N_T \end{aligned}$$

- 20 If we assume that  $Q = N'_p/N_T$ , column  $n = q + (\mu-1)Q$  of the CIR is given by  $\{\tilde{h}'_I\}_n = \tilde{h}_{I,q}^{(\mu)}$ . Otherwise, if  $Q < N'_p/N_T$ , the size of the channel impulse response can be matched by zero padding. Hence, the following equation follows readily

$$25 \quad \zeta_I = \tilde{h}'_I + \tilde{n}'_I = \hat{h}'_{LS_I} \quad N'_p \geq N_T Q$$

where  $\tilde{n}'_I = 1/N'_p \tilde{F}^H \tilde{N}'_I$  denotes the IDFT of the AWGN realisation  $\tilde{N}'_I$ , which is itself a white Gaussian noise process with the same variance. This means that the  $N_T$  superimposed

- 30 signals are completely separated, provided that  $N'_p \geq N_T Q$ .

5 The MMSE estimator is in general dependent on the choice of the pilot symbols. However, choosing appropriate pilot sequences, the estimator becomes independent of the transmitted pilots. It is desirable to choose a set of pilot sequences, which minimises the mean squared error  
 10 (i.e. the performance of the estimator) and the computational complexity of the estimator. Hence, if the pilot sequences are appropriately chosen, the least squares estimator as well as the minimum mean square error estimator can be grossly simplified.

15

In order to generate the MMSE estimator, a knowledge of the correlation matrices  $R'_{\zeta\zeta}$  and  $R'_{h\zeta}$  are required. For the derivation of the Wiener filter it is assumed that  $Q = N'_p / N_T$ . Otherwise, the size of the channel impulse  
 20 response can be matched by zero padding. The MMSE estimates for OFDM symbols is given by (S.M. Kay, "Fundamentals of Statistical Signal Processing: Estimation Theory", Englewood Cliffs, NJ: Prentice Hall International, 1993)

25

$$\hat{h}'_I = R'_{h\zeta} R'^{-1}_{\zeta\zeta} \zeta'_I = \frac{1}{N'_p} w' \tilde{F}^H \tilde{Y}'_I$$

$$w' = R'_{h\zeta} R'^{-1}_{\zeta\zeta} \in \mathbb{C}^{N'_h \times N'_p}$$

30 where the correlation matrices  $R'_{\zeta\zeta}$  and  $R'_{h\zeta}$  are defined by



$$\begin{aligned}
R'_{\zeta\zeta} &\stackrel{\Delta}{=} E\{\zeta'_T \zeta'^{H}_T\} = \frac{1}{N'^2_P} \tilde{F}^H R'_{yy} \tilde{F} \in \mathbb{C}^{N'_T \times N'_T} \\
&= R'_{hh} + \frac{N_0}{N'_P} I
\end{aligned}$$

and

$$\begin{aligned}
R'_{h\zeta} &\stackrel{\Delta}{=} E\{h'_T \zeta'^{H}_T\} \in \mathbb{C}^{N'_T \times N'_P} \\
&= R'_{\tilde{h}\tilde{\zeta}}
\end{aligned}$$

In order to perform MIMO OFDM channel estimation in time direction, by appropriately scaling of the parameters, the same inventive algorithms for channel estimation can be applied to DFT-based channel estimation in time direction.

In the following, the system model for equalization of  $N_T$  superimposed pilot signals in time direction, i.e. the received pilot sequence of tone  $\tilde{t}$  of  $N'_P$  OFDM symbols is introduced. Considering channel estimation in time direction, the pilots  $[Y_{1,j}, Y_{D,j}, \dots, Y_{D, N'_P, j}] \in \mathbb{G}$  are used in order to estimate  $\hat{H}_{t,j}^{(\mu)}$ . In vector notation, the received pilot sequence of tone  $\tilde{t}$  is defined by

$$\begin{aligned}
\tilde{Y}''_{\tilde{t}} &= \sum_{\mu=1}^{N_T} \tilde{X}''_{\tilde{t}}^{(\mu)} \tilde{H}''_{\tilde{t}}^{(\mu)} + N''_{\tilde{t}} \in \mathbb{C}^{N'_T \times 1} \\
&= \tilde{X}''_{\tilde{t}} \tilde{H}''_{\tilde{t}} + N''_{\tilde{t}}
\end{aligned}$$

5

where the transmitted pilots, the general transfer  
function, the general impulse response and the additive  
10 noise components are given by

$$\begin{aligned}\tilde{X}_T'' &= [\tilde{X}_T''(0), \dots, \tilde{X}_T''(N_T)] \in \mathbb{C}^{N_p \times N_p N_T}, & \tilde{X}_T''(\mu) &= \text{diag}(\tilde{X}_{1,T}^{(\mu)}, \dots, \tilde{X}_{N_p,T}^{(\mu)}) \in \mathbb{C}^{N_p \times N_p} \\ \tilde{H}_T'' &= [\tilde{H}_T''(0)^T, \dots, \tilde{H}_T''(N_T)^T]^T \in \mathbb{C}^{N_p N_T \times 1}, & \tilde{H}_T''(\mu) &= [\tilde{H}_{1,T}^{(\mu)}, \dots, \tilde{H}_{N_p,T}^{(\mu)}]^T \in \mathbb{C}^{N_p \times 1} \\ \tilde{N}_T'' &= [\tilde{N}_{1,T}, \dots, \tilde{N}_{N_p,T}]^T \in \mathbb{C}^{N_p \times 1}\end{aligned}$$

15

There are two scenarios which will be considered: first,  
20 burst like transmission where a frame of an OFDM symbol is  
transmitted; second, a broadcasting scenario with a  
continuously transmitted data stream. In burst transmission  
mode, L OFDM symbols are received, buffered, and after  
reception is complete, the whole frame is processed. This  
25 is the same as for the channel estimation in frequency  
direction, where all pilots of one OFDM symbol are being  
received together as well. The difference is that the  
algorithms which were applied dependent on the  $i$  variable  
are now used in the  $l$  variable. That is, the received pilot  
30 is transformed into the Doppler domain via an IFFT. The  
least squares and minimum mean squared error estimator work  
exactly in the same way as the previously discussed case of  
channel estimation in frequency direction.

5 Referring to the broadcasting scenario, for continuous transmission there are some differences with respect to the channel estimation in frequency direction. Some buffering is usually possible since receiving the whole sequence before processing is sometimes not feasible.  $L = D_t N_p''$  is  
10 defined as the number of OFDM symbols, which are in the input buffer. For smoothing type filtering as described by S.M. Kay, "Fundamentals of Statistical Signal Processing: Estimation Theory", Englewood Cliffs, NJ: Prentice Hall International, 1993, we use past as well as future pilots  
15 to estimate  $\hat{H}_{t,i}^{(u)}$ . This means  $1 < l < D_t N_p''$ . Clearly, for smoothing an estimate cannot be obtained until all pilots have been received, which requires buffering of  $\Delta l = D_t N_p'' - l$  OFDM symbols. The alternative is to use prediction type filtering where  $l > D_t N_p''$ . In this case only past pilots are  
20 used for channel estimation in time direction. Obviously, prediction type filtering does not require any buffering, however, the performance with respect to smoothing degrades.

25 The major difference with respect to channel estimation in frequency direction is that only  $D_t$  symbols per sub-carrier are output at a time, i.e., an input of  $N_p''$  pilots is used to produce an output of  $D_t$  symbols per sub-carrier. Furthermore, the number of pilots in time direction is  
30 usually significantly smaller than the number of pilots in frequency direction, but the pilot spacing frequency in time direction is similar. Since  $N_p''' \ll N_p'$  the leakage of the Doppler domain transform will be more significant. On the other hand, when only the symbols in the centre of the  
35 processed pilots are used, the performance may be improved,

5 since the estimation error is typically much lower at the centre compared to the area near the edges.

Up to now much of discussion is dealing with 1D channel estimation in frequency direction over one OFDM symbol in  
10 the  $i$  variable. The proposed techniques are, however, also applicable to channel estimation in time direction in a straight forward way (i.e. estimating in the  $l$  variable). Moreover, an extension to a multi carrier system with correlations in two dimensions is possible by using two  
15 cascaded one dimensional Wiener filters. This idea has been suggested for SISO channel estimation by e.g. P. Hoeher, S. Kaiser, and P. Robertson, "Two-Dimensional Pilot-Symbol-Aided Channel Estimation by Wiener Filtering", in Proc. IEEE Intern. Conf. On Acoustics, Speech, and Signal  
20 Processing. (ICASSP'97), Munich, Germany pp. 1845-1848, 1997, and can be extended to the MIMO case.

The inventive apparatus for estimating a plurality of channels is operative to translate phase shifts into delays  
25 in order to estimate channel information, i.e. a channel impulse response of one of a plurality of communication channels. Hence, phase shifted sequences are perfectly suitable for channel estimation. Moreover, also other orthogonal sequences can be applied to channel estimation,  
30 as long as the pilot symbols have a particular phase shift characteristic with respect to other pilot symbols. That means, that the phase shift between two pilot sequences may vary following a predetermined function so that for example a first half of a first pilot sequence has a phase shift  
35 with respect to a first half of a second pilot sequence and a second half of the pilot sequence has a further phase shift with respect to a second half of the second pilot

- 5 sequence. Therefore, the phase shift characteristics of the pilot sequences can be exploited at the transmitting points to estimate the channel by applying for example the inventive low complexity channel estimation scheme.
- 10 As an example of orthogonal sequences, the properties of Hadamard sequences are studied. For a system with  $N_T$  transmit antennas a set Hadamard basis function of order  $N_T$ , denoted by  $H$  is used. In order to generate  $\tilde{X}_T^{(\mu)}$ , the  $\mu^{\text{th}}$  column of these basis functions are periodically extended
- 15 to pilot sequence length  $N'_p$ , as discussed above. For example, for  $N_T=2$  the Hadamard sequences are identical to the phase shifted sequences, i.e.  $\tilde{X}_T^{(0)}$  is the all one sequence, and the second sequence is oscillating between 1 and -1, i.e.  $\tilde{X}_T^{(2)} = [1, -1, 1, \dots, -1]^T$ . If  $N_T=4$ , the Hadamard
- 20 sequences can be cast into the matrix

$$H_4 = \begin{bmatrix} 1 & 1 & 1 & 1 \\ 1 & -1 & 1 & -1 \\ 1 & 1 & -1 & -1 \\ 1 & -1 & -1 & 1 \end{bmatrix}$$

25

- It is easy to clarify that  $H_4$  is symmetric and orthogonal i.e.  $H_4 = H_4^T$  and  $H_4 \cdot H_4^T = 4 \cdot I$ . In case that  $N_T=4$ , the received pilot sequence transformed into the time domain, is defined
- 30 by  $\zeta_T = 1/N'_p \tilde{F}^H \tilde{Y}'_T$ . It will be shown, that the least squares estimators for transmit antennas 1, ..., 4 is given by

$$\begin{aligned}
\hat{h}_{LS_T}^{(1)} &= \zeta_T^{(1)} = \tilde{h}_T^{(1)} + \tilde{n}_{t_1}' \\
\hat{h}_{LS_T}^{(2)} &= \zeta_T^{(2)} = \tilde{h}_T^{(2)} + \tilde{n}_{t_2}' \\
\hat{h}_{LS_T}^{(3)} &= e^{-j\pi/4} \zeta_T^{(2)} + e^{-j\pi/4} \zeta_T^{(4)} = \tilde{h}_T^{(3)} + \tilde{n}_{t_3}' \\
\hat{h}_{LS_T}^{(4)} &= e^{-j\pi/4} \zeta_T^{(2)} + e^{-j\pi/4} \zeta_T^{(4)} = \tilde{h}_T^{(4)} + \tilde{n}_{t_4}'
\end{aligned}$$

10 where  $\zeta_T^{(\mu)}$  accounts the part of  $\zeta_T$ , assuming that  $\zeta_T$  is  
 divided into  $N_T$  equal parts, i.e.  $\zeta_T = [\zeta_T^{(1)T}, \dots, \zeta_T^{(N_T)T}]^T$ .  
 Furthermore,  $\tilde{n}_{t,\mu}'$  denotes the resulting noise term of  $\mu^{\text{th}}$   
 part. It is seen that the signal of antenna 2 is received  
 in partition 3. This may be confusing and can be fixed by  
 15 exchanging columns 2 and 3 of  $H_{NT}$ .

To apply the above simplification of the receiver structure  
 with pilot sequences based on Hadamard codes, additional  
 processing may be necessary. For the case  $N_T=4$  and pilot  
 20 sequence is based on Hadamard codes, the receiver structure  
 of the FFT is derived. The starting point is the received  
 pilot sequence transformed into time domain given by  
 $\zeta_T = 1/N_p \tilde{F}^H \tilde{Y}_T'$ . The DFT of the pilot sequence  $\tilde{X}_{T,i}^{(\mu)}$  for  
 transmit antenna 1, ..., 4 can  
 25 be expressed as

$$\begin{aligned}
F_{N'_p}(\tilde{X}_{\tilde{l},\tilde{l}}^{(1)})_{q-n} &= N'_p \delta_{n-q} \\
F_{N'_p}(\tilde{X}_{\tilde{l},\tilde{l}}^{(2)})_{q-n} &= N'_p \delta_{n-q-N'_p/2} \\
5 \quad F_{N'_p}(\tilde{X}_{\tilde{l},\tilde{l}}^{(3)})_{q-n} &= \frac{N'_p}{2} \cdot (e^{j\pi/4} \delta_{n-q-N'_p/4} + e^{-j\pi/4} \delta_{n-q-N'_p 3/4}) \\
F_{N'_p}(\tilde{X}_{\tilde{l},\tilde{l}}^{(4)})_{q-n} &= \frac{N'_p}{2} \cdot (e^{-j\pi/4} \delta_{n-q-N'_p/4} + e^{j\pi/4} \delta_{n-q-N'_p 3/4})
\end{aligned}$$

10 Hence, it can be observed that the signal from antenna 1 is identical to the case of phase shifted sequences are used, and the signal from antenna 3 is the same as the signal from antenna 2 in the above equation, which corresponds to the least squares (LS) estimate. This is due to the  
 15 inventive arrangements of the codes and may be fixed by exchanging for example columns 2 and 3. The DFT of pilots 3 and 4 in the above equation consists of two impulses which interfere with each other. Furthermore, the DFT of pilot 3,  $F_{N'_p}(\tilde{X}_{\tilde{l},\tilde{l}}^{(3)})_{q-n}$ , is the conjugate complex of  $F_{N'_p}(\tilde{X}_{\tilde{l},\tilde{l}}^{(4)})_{q-n}$ . Hence,

20

$$\zeta_{\tilde{l},n} = \begin{cases} \tilde{h}_{\tilde{l},n}^{(1)} + \tilde{n}_{\tilde{l},n}, & n = \{1, \dots, \frac{1}{4} N'_p\} \\ e^{j\pi/4} \tilde{h}_{\tilde{l},n}^{(3)} + e^{-j\pi/4} \tilde{h}_{\tilde{l},n}^{(4)} + \tilde{n}_{\tilde{l},n}, & n = \{\frac{1}{4} N'_p + 1, \dots, \frac{1}{2} N'_p\} \\ \tilde{h}_{\tilde{l},n}^{(2)} + \tilde{n}_{\tilde{l},n}, & n = \{\frac{1}{2} N'_p + 1, \dots, \frac{3}{4} N'_p\} \\ e^{-j\pi/4} \tilde{h}_{\tilde{l},n}^{(3)} + e^{j\pi/4} \tilde{h}_{\tilde{l},n}^{(4)} + \tilde{n}_{\tilde{l},n}, & n = \{\frac{3}{4} N'_p + 1, \dots, N'_p\} \end{cases}$$

25

5    where again it is assumed that  $Q \leq N'_p/N_T$ . Removing the  
inserted phase shift of the pilots and adding the two-parts  
of the signal, the equation to-be shown follows readily.

10    In practice, two times oversampling provides a good trade  
of between minimising the system overhead due to pilots and  
optimising the performance. It is assumed that the length  
of the guard interval is not smaller than  $Q$ , i.e. the guard  
interval is not shorter than the maximum delay of the  
channel.

15    Moreover, depending on certain implementation requirements  
of the inventive method for estimating a plurality of  
channels or for providing a plurality of different pilot  
sequences can be implemented in hardware or in software.  
20    The implementation can be performed using a digital storage  
medium, in particular a disc or a CD having electronically  
readable control signals stored thereon, which can  
cooperate with a programmable computer system such that the  
inventive methods are performed. Generally, the present  
25    invention is, therefore, a computer-program product with a  
program code stored on a machine-readable carrier, the  
program code being for performing the inventive methods,  
when the computer program product runs on a computer. In  
other words, the inventive method is, therefore, a computer  
30    program having a program code for performing the inventive  
methods, when the computer program runs on a computer.



5    CLAIMS

1.    Apparatus for estimating a plurality of channels from a plurality of distinct transmitting points to a receiving point, wherein an input signal includes  
10    a superposition of a first signal based on a first pilot sequence transmittable from a first transmitting point and a second signal based on a second pilot sequence transmittable from a second transmitting point, the first pilot sequence and  
15    the second pilot sequence being orthogonal to each other within a predetermined orthogonality range and having a phase shift to each other, comprising:
- 20    a transformer (103; 303) for transforming the input signal into a transformed signal having a set of discrete values, the transformer (103; 303) being operative to translate the phase shift between the first and the second pilot sequence into a delay, so that a first group of the set of the discrete  
25    values includes channel information of a first channel from the first transmitting point to the receiving point and that a second group of the set of discrete values includes channel information of a second channel from the second transmitting point  
30    to the receiving point;
- 35    a selector (105; 305) for selecting the first group from the set of discrete values and for selecting the second group from the set of discrete values to obtain selected groups; and
- means    (107;    315)    for    determining    channel

5 information for the plurality of channels based on the selected groups.

2. Apparatus in accordance with claim 1, wherein the input signal includes, in a superimposed manner, a  
10 third signal based on a third pilot sequence transmittable from a third transmitting point, the third pilot sequence being orthogonal to the first and the second pilot sequences within the orthogonality range, and having a further phase  
15 shift to the first pilot sequence, the transformer (103; 303) being further operative to translate the further phase shift into a further delay, so that a third group of the set of discrete values includes channel information of a third channel from the  
20 third transmitting point to the receiving point; and

wherein the selector (105; 305) is operative to further select the third group from the set of  
25 discrete values to obtain a selected third group.

3. Apparatus in accordance with claim 1 or 2, wherein each group consists of an equal number of successive discrete values of the set of discrete  
30 values.

4. Apparatus in accordance with any one of the preceding claims, wherein the transformer is operative to perform a Fourier transform or a fast  
35 Fourier transform or a discrete Fourier transform or an inverse Fourier transform or an inverse fast

- 5           Fourier transform or an inverse discrete Fourier transform on the input signal.
- 10           5. Apparatus in accordance with any one of the preceding claims, wherein the set of discrete values includes a total number of discrete values, the number being obtained by the transformer (103; 303).
- 15           6. Apparatus in accordance with claim 5, in which the plurality of transmitting points has a total number of transmitting points, wherein the selector (105; 305) is operative to select, as a group, a number of successive discrete values, the number being equal to the total number of discrete values divided by the total number of transmitting points.
- 20           7. Apparatus in accordance with claim 6, in which the selector (105; 305) is operative to select the groups such that a first discrete value of the set of discrete values is a first discrete value in the first group and a first discrete value of the second group of discrete values is a discrete value in the set of discrete values succeeding a discrete value having a highest order of the values selected to obtain the first group.
- 25           8. Apparatus in accordance with any one of the preceding claims, in which the input signal is a set of successive input signal values, and in which the transformer (103; 303) is operative to transform the set of successive input signal values into the set of discrete values, wherein a total
- 30           35

- 5           number of discrete values of the set of discrete  
values is equal to a total number of input signal  
values in the set of input signal values.
- 10           9. Apparatus in accordance with any one of the  
preceding claims, in which the transformer (103;  
303) is operative to perform a transform algorithm,  
and in which the set of discrete values is  
generated by a single execution of the transform  
algorithm by the transformer.
- 15           10. Apparatus in accordance with claim 9, in which the  
transform algorithm being performed by the  
transformer (103; 303) is a Fourier transform or a  
fast Fourier transform or a discrete Fourier  
20           transform or an inverse Fourier transform or an  
inverse fast Fourier transform or an inverse  
discrete Fourier transform algorithm applied to the  
total number of input signal values.
- 25           11. Apparatus in accordance with any one of the  
preceding claims, wherein the pilot sequences  
include a complex amplitude sequence and phase  
information, wherein the complex amplitude sequence  
is the same for the pilot sequences, comprising:
- 30           a multiplier (101) being operative to multiply a  
received signal by a complex-conjugated version of  
the amplitude sequence to obtain the input signal.
- 35           12. Apparatus in accordance with claim 11, wherein the  
received signal is a set of successive discrete  
received signal values and wherein the complex

5           conjugated version of the amplitude sequence is a set of successive discrete complex conjugated amplitude signal values, and

10           wherein the multiplier (101) is operative to perform a single complex multiplication for a value of the set of successive discrete signal values and a corresponding value of the set of successive discrete complex conjugated amplitude signal values, so that after a number of single  
15           multiplications the set of successive discrete input values is obtained.

13. Apparatus in accordance with any one of the preceding claims, in which the means (107; 315) for  
20           determining channel information is operative to receive the selected groups and to output the selected groups, each group of the selected groups including channel information of a particular channel.

25           14. Apparatus in accordance with claim 13, wherein the means (107; 315) for determining channel information is operative to determine the channel information by outputting the selected groups, each  
30           group including channel impulse responses of a particular channel as channel information.

35           15. Apparatus in accordance with claim 13, wherein the means (107; 315) for determining channel information includes a time/frequency conversion means for obtaining a channel transfer function as the channel information.

5

16. Apparatus in accordance with any one of the preceding claims, wherein a group of the selected groups and a further group of the selected groups include channel information of a channel and channel information of a further channel in a super imposed manner, wherein the means (107; 315) for determining channel information is operative to determine the channel information of the channel and the channel information of the further channel based on the group and on the further group.

10

17. Apparatus in accordance with claim 16, wherein a group of the selected groups includes a superposition of the channel information of a channel being multiplied by a phase shift factor and of a further channel information of a further channel being multiplied by a further phase shift factor, and

20

wherein a further group of the selected groups includes a superposition of the channel information of the channel being multiplied by the complex conjugated phase shift factor and of the further channel information of the further channel being multiplied by the complex-conjugated further phase shift factor, the phase shift factor and the further phase shift factor being caused by the pilot sequences, wherein

25

30

the means (107; 315) for determining channel information is operative to determine the channel information of the channel and the channel

35

- 5           information of the further channel using the group  
and the further group.
18. Apparatus in accordance with claim 17, wherein the  
means (107; 315) for determining channel  
10       information is operative to determine the channel  
information and the further channel information  
using phase shift operations and addition and/or  
subtraction operations applied to the group and to  
the further group.
- 15       19. Apparatus in accordance with claim 17 or 18,  
wherein the phase shift factor is a function of a  
phase shift of 180 degrees divided by the total  
number of transmitting points.
- 20       20. Apparatus in accordance with any one of the  
preceding claims, wherein a channel information is  
corrupted by a distortion signal, the means (107;  
315) for determining further comprising an  
25       estimator being operative to estimate the channel  
information from the corrupted channel information.
- 30       21. Apparatus in accordance with claim 20, wherein the  
estimator is operative to perform a minimum mean  
squared error estimation or a maximum a posteriori  
estimation or a maximum likelihood estimation for  
providing an estimated channel information.
- 35       22. Apparatus in accordance with any one of the  
preceding claims, in which the pilot sequences are  
used to modulate a discrete carrier in a multi

5 carrier modulation scheme at a predetermined time instant, the apparatus further comprising:

a controller for detecting the input signal in a received signal and for enabling the transformer  
10 (103; 303), the selector (105; 305) or the means (107; 315) for determining only when the input signal is detected in the received signal.

23. Apparatus in accordance with any one of the  
15 preceding claims, in which the pilot sequences are used to modulate the same pilot carrier in a multi carrier modulation scheme at distinct transmitting time instants, the apparatus further comprising:

20 a controller for detecting a pilot carrier in a received signal including successive multi carrier modulated symbols and for collecting values of the pilot carrier at time instants corresponding to transmitting instants to obtain the input signal,  
25 wherein the channel information obtained by processing the input signal using the transformer (103; 303), the selector (105; 305) and the means (107; 315) for determining includes information on a multi carrier channel from transmitting points to  
30 receiving point defined by the pilot carrier over time.

24. Apparatus in accordance with any one of the  
35 preceding claims, wherein the apparatus further comprises a single means (301) for windowing the input signal to obtain a windowed input signal to



5           be used as the input signal for the transformer  
          (103; 305).

25. Apparatus for providing a plurality of different  
pilot sequences to be used for channel estimation,  
10           comprising:

          means (401) for calculating an  $i^{\text{th}}$  value  $X_i^{(\mu)}$  of a  
pilot sequence to be transmitted by a  $\mu^{\text{th}}$   
transmitting point of  $N_T$  transmitting points using  
15           the                           following                           equation:

$$X_i^{(\mu)} = e^{-j2\pi(i-1)(\mu-1)/N_T} X_i^{(s)}$$

20           wherein  $N_T$  denotes a number of transmitting points  
and wherein  $N_T$  is greater than or equal to 3; and

          wherein  $X_i^{(s)}$  denotes an  $i^{\text{th}}$ , value of a scrambling  
sequence, the length of the scrambling sequence  
25           being equal to the length of the pilot sequence.

26. Apparatus for providing a number of different pilot  
sequences to be used for channel estimation,  
          comprising:

30           means (501) for generating a Hadamard matrix having  
a number of columns, the number of columns  
corresponding to the number of different pilot  
sequences;

35           means (503) for calculating the different pilot  
sequences based on the columns of the Hadamard

5           matrix, wherein each pilot sequence is derived from  
another column of the Hadamard matrix.

27. Method for estimating a plurality of channels from  
a plurality of distinct transmitting points to a  
10       receiving point, wherein an input signal includes a  
superposition of a first signal based on a first  
pilot sequence transmittable from a first  
transmitting point and a second signal based on a  
second pilot sequence transmittable from a second  
15       transmitting point, the first pilot sequence and  
the second pilot sequence being orthogonal to each  
other within a predetermined orthogonality range  
and having a phase shift to each other, comprising  
the following steps:

20       transforming the input signal into a transformed  
signal having a set of discrete values by  
translating the phase shift between the first and  
the second pilot sequence into a delay, so that a  
25       first group of the set of discrete values includes  
channel information of a first channel from the  
first transmitting point to the receiving point and  
that a second group of the set of discrete values  
includes channel information of a second channel  
30       from the second transmitting point to the receiving  
point;

      selecting the first group from the set of discrete  
values and selecting the second group from the set  
35       of discrete values to obtain selected groups;

5

determining channel information for the plurality of channels on the basis of the selected groups.

28. Method for providing a plurality of different pilot sequences to be used for channel estimation, comprising the following steps:

10

15

Calculating an  $i^{\text{th}}$  value value  $X_i^{(\mu)}$  of a pilot sequence to be transmitted by a  $\mu^{\text{th}}$  transmitting point of  $N_T$  transmitting points using the following equation:

$$X_i^{(\mu)} = e^{-j2\pi(i-1)(\mu-1)/N_T} X_i^{(s)}$$

20

wherein  $N_T$  denotes a number of transmitting points and wherein  $N_T$  is greater than or equal than 3; and

25

wherein  $X_i^{(s)}$  denotes an  $i^{\text{th}}$  value of a scrambling sequence, the length of which being equal to the length of the pilot sequences.

29. Method for providing a number of different pilot sequences to be used for channel estimation, comprising the following steps:

30

generating a Hadamard matrix having a number of columns, the number of columns corresponding to the number of different pilot sequences;

35

calculating the different pilot sequences based on the columns of the Hadamard matrix, wherein each

5 pilot sequence is derived from another column of  
the Hadamard matrix.

30. Computer program having a program code for  
performing the method for estimating a plurality of  
10 channels in accordance with claim 27, the method  
for providing a plurality of pilot sequences in  
accordance with claim 28, the method for providing  
a plurality of pilot sequences in accordance with  
claim 29, when the program runs on a computer.

15

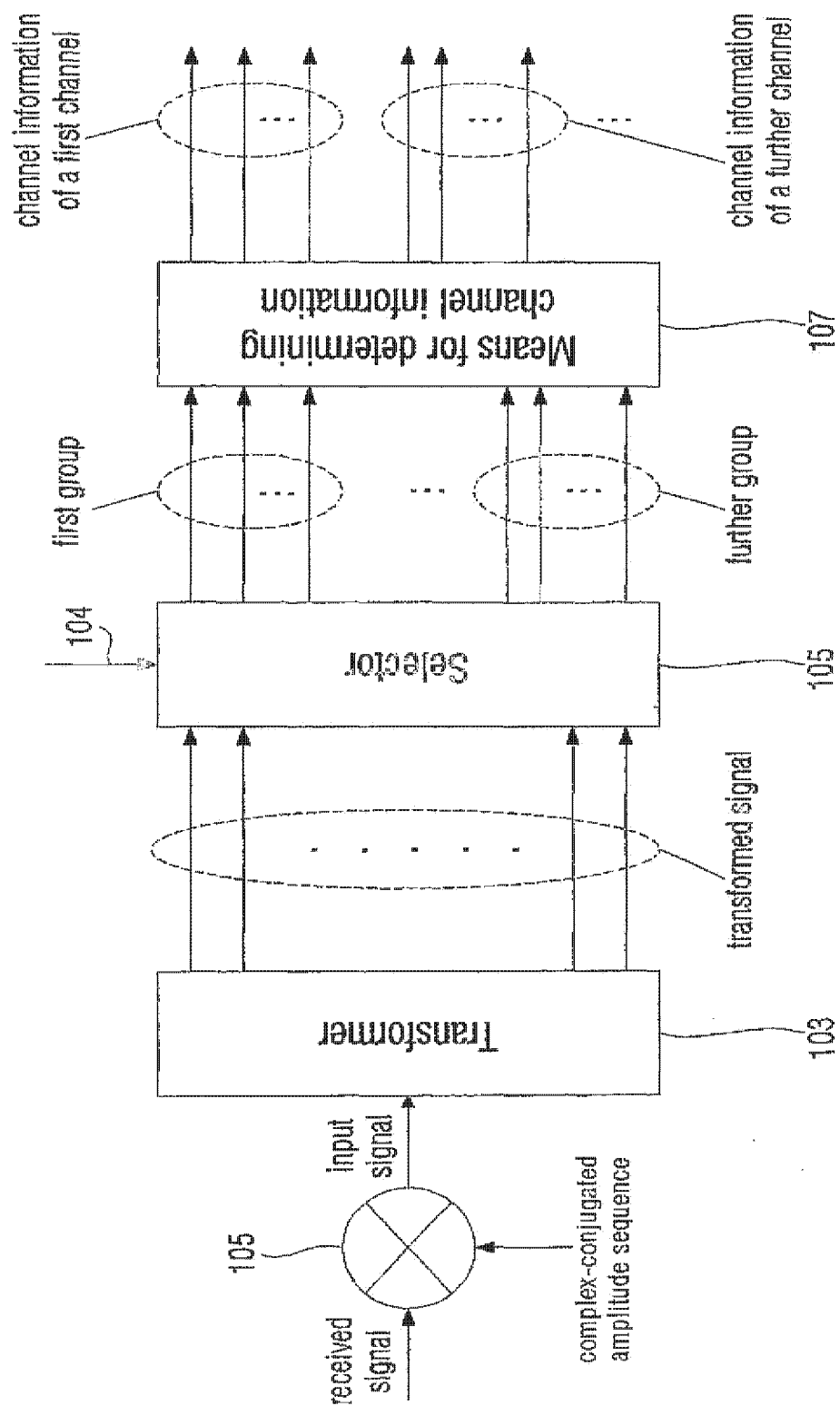


FIG. 1

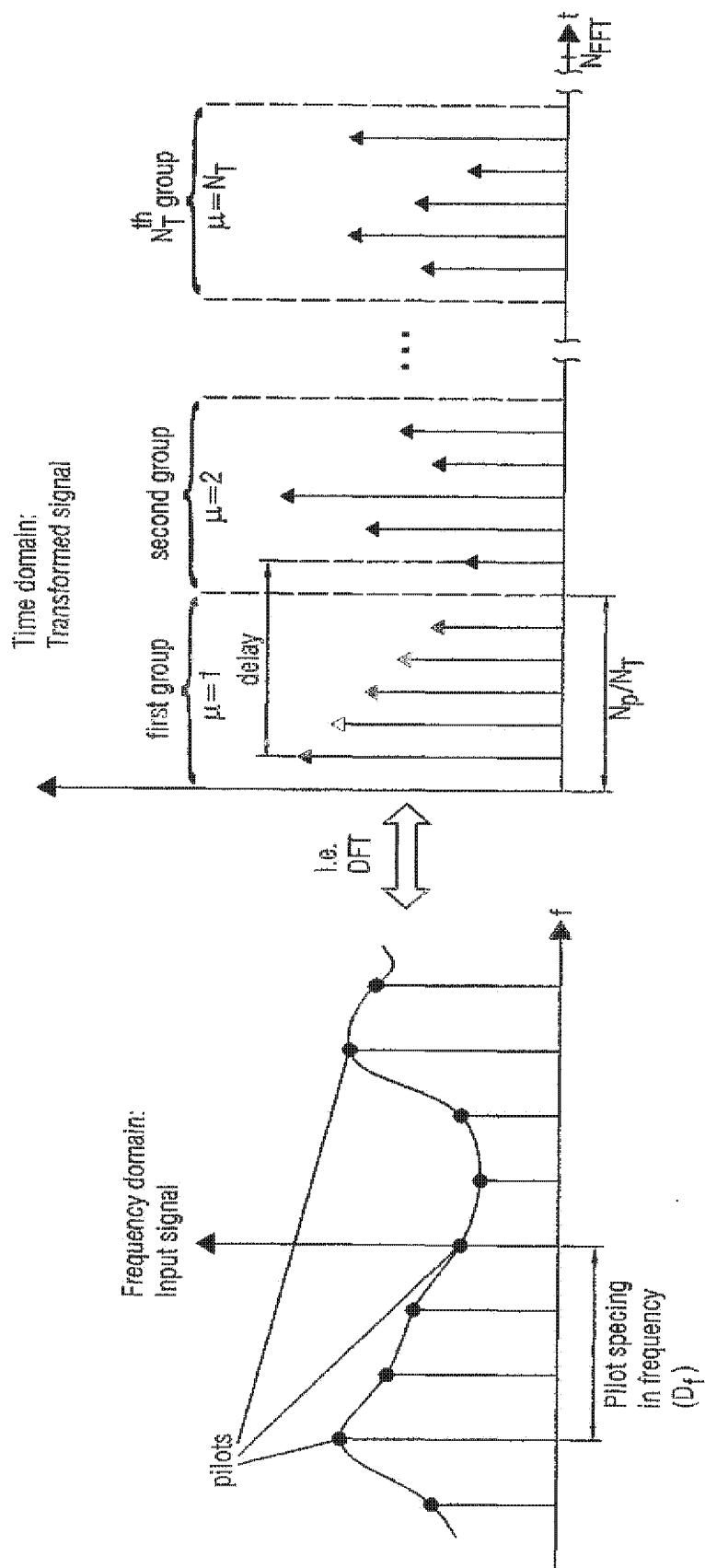


FIG. 2

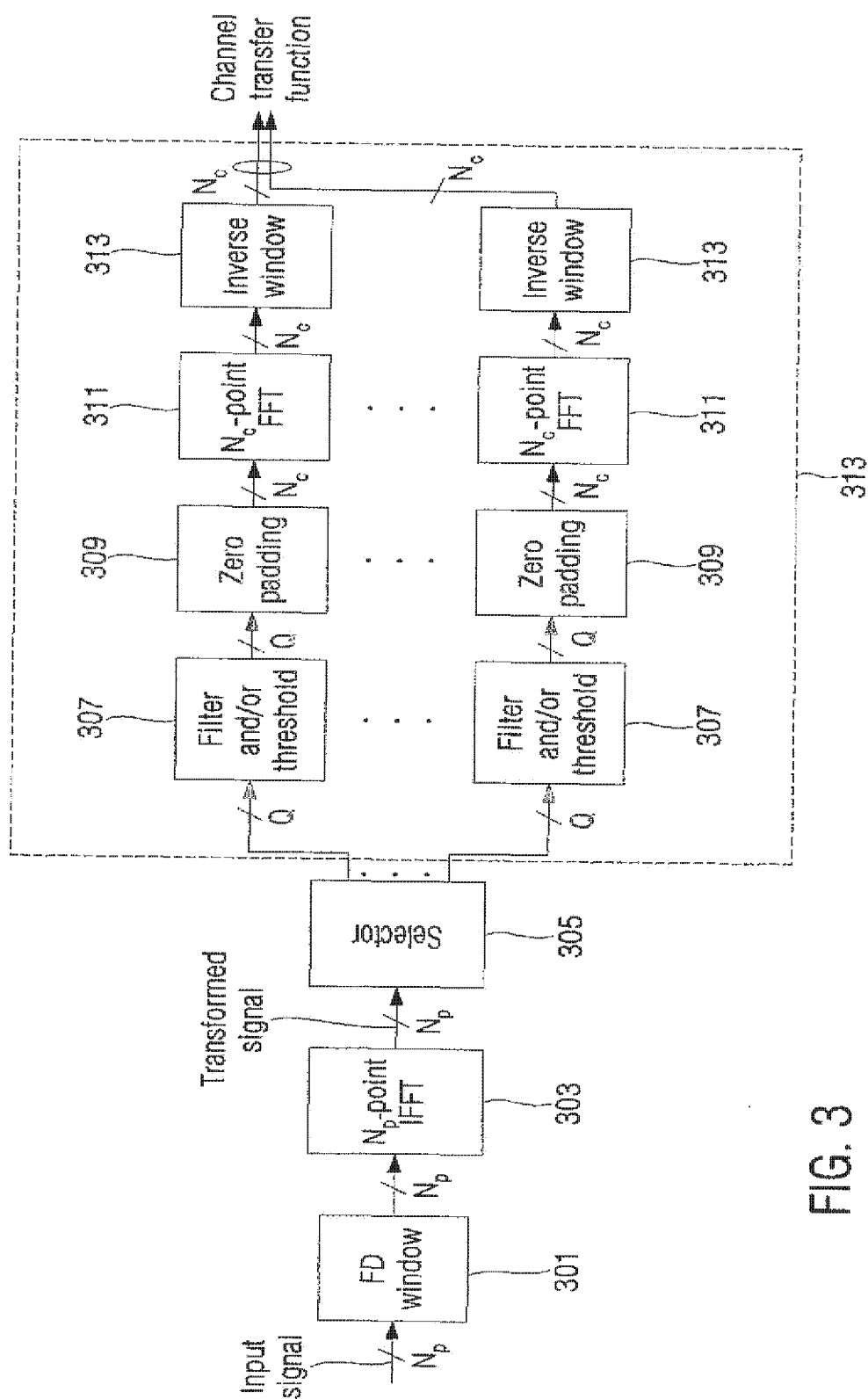
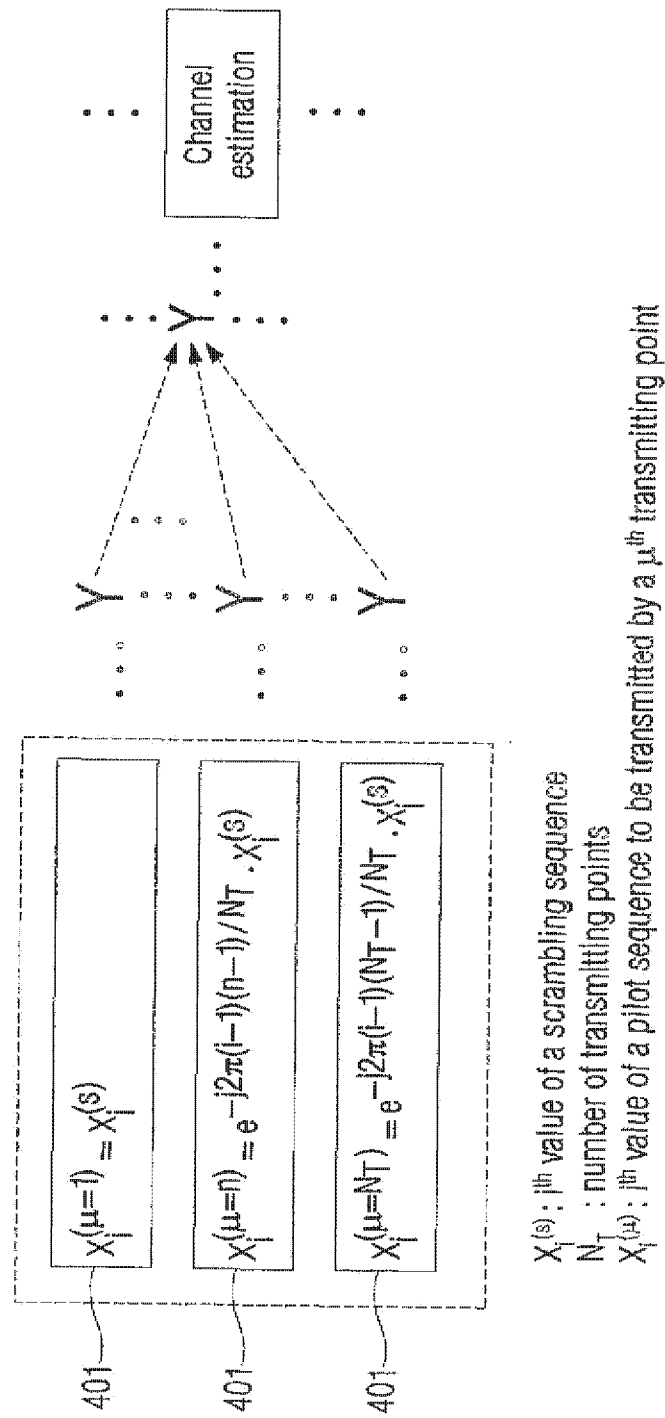


FIG. 3

FIG. 4





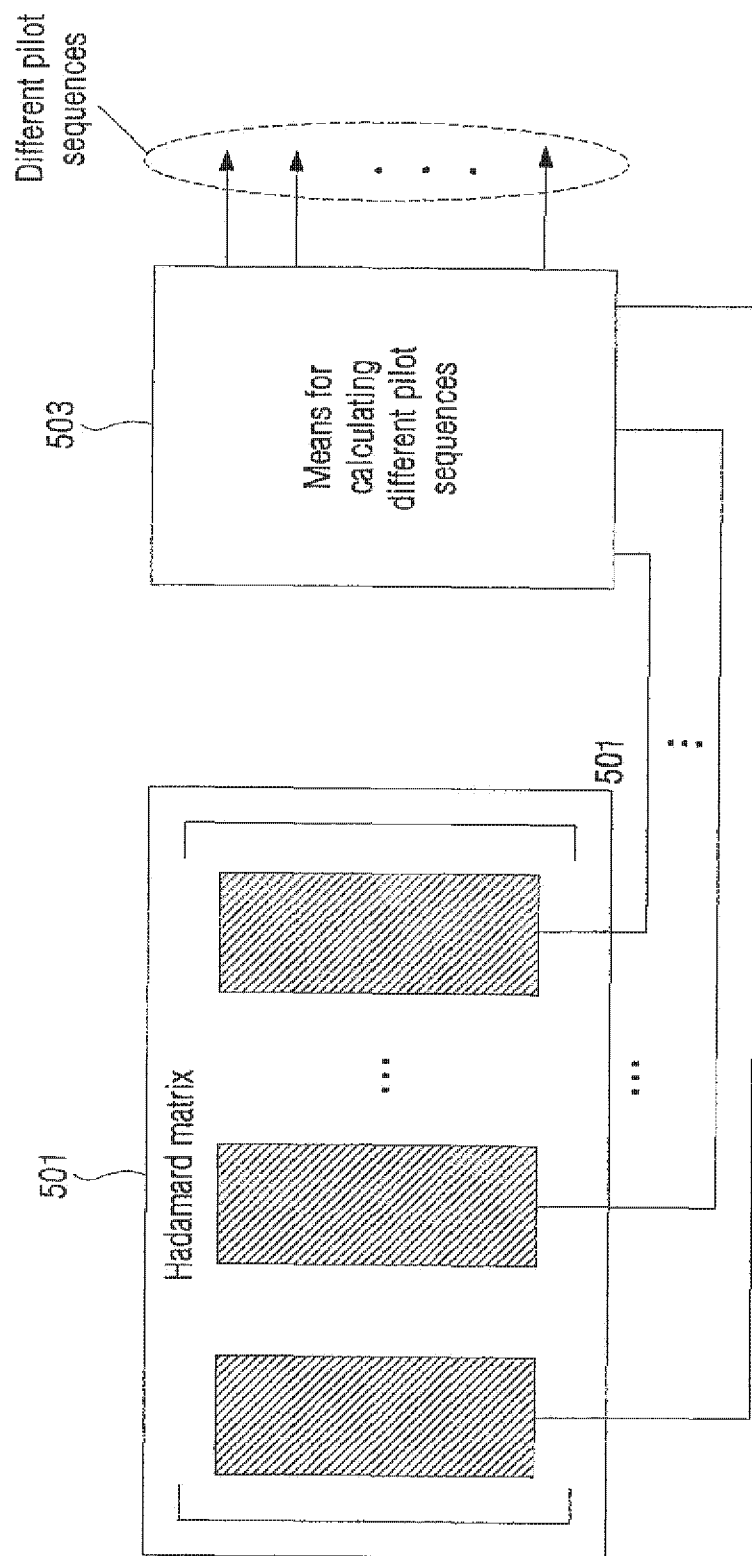


FIG. 5

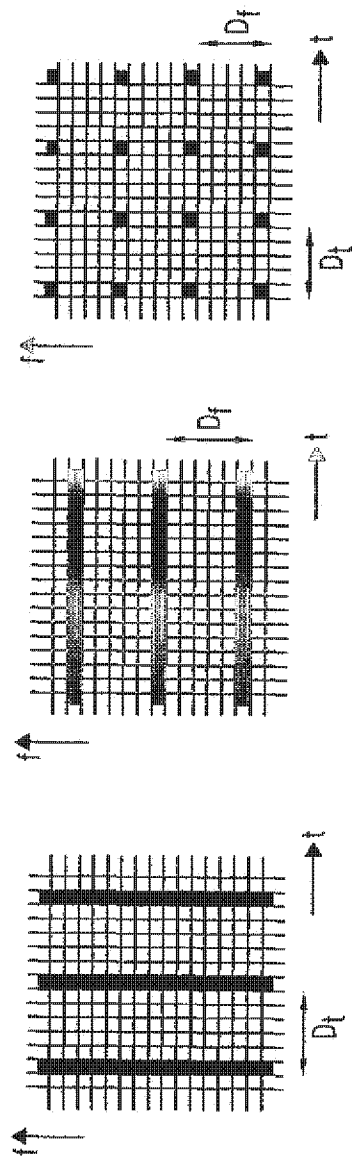


FIG. 6

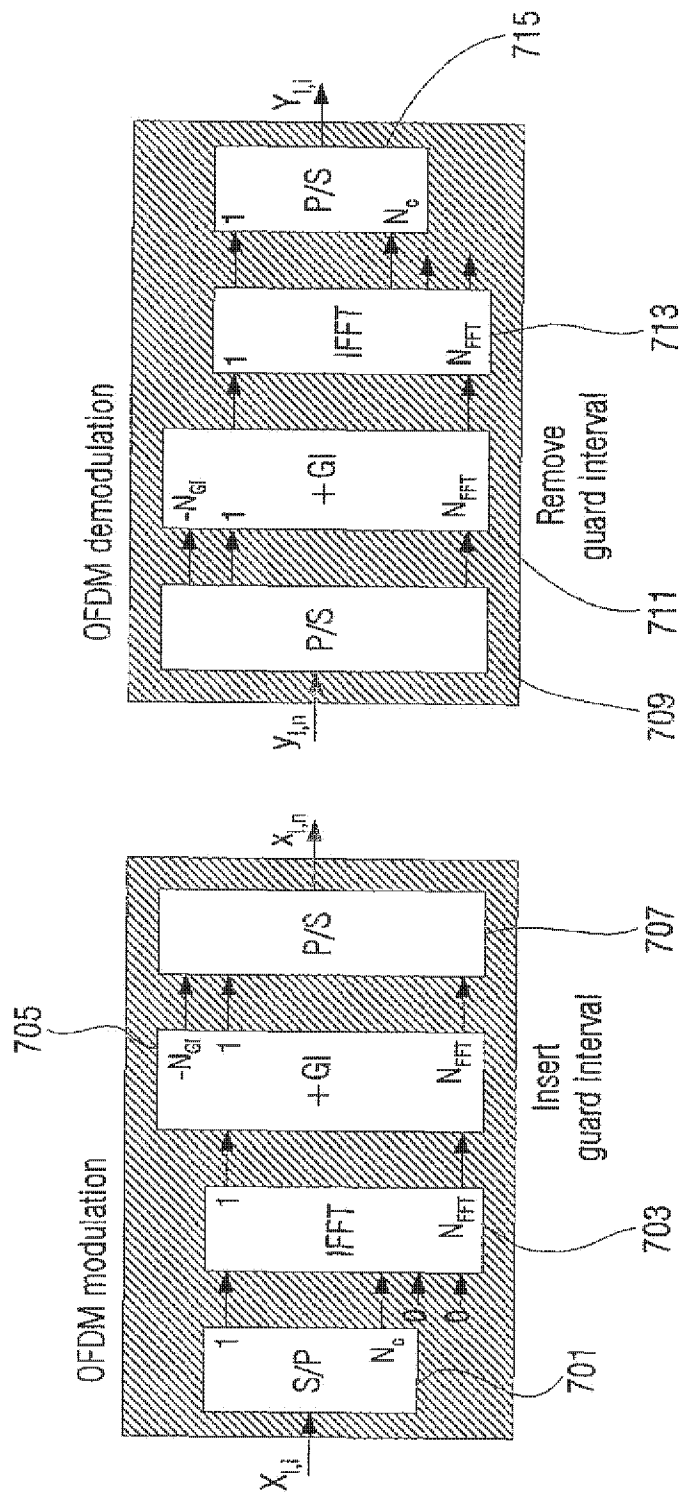


FIG. 7

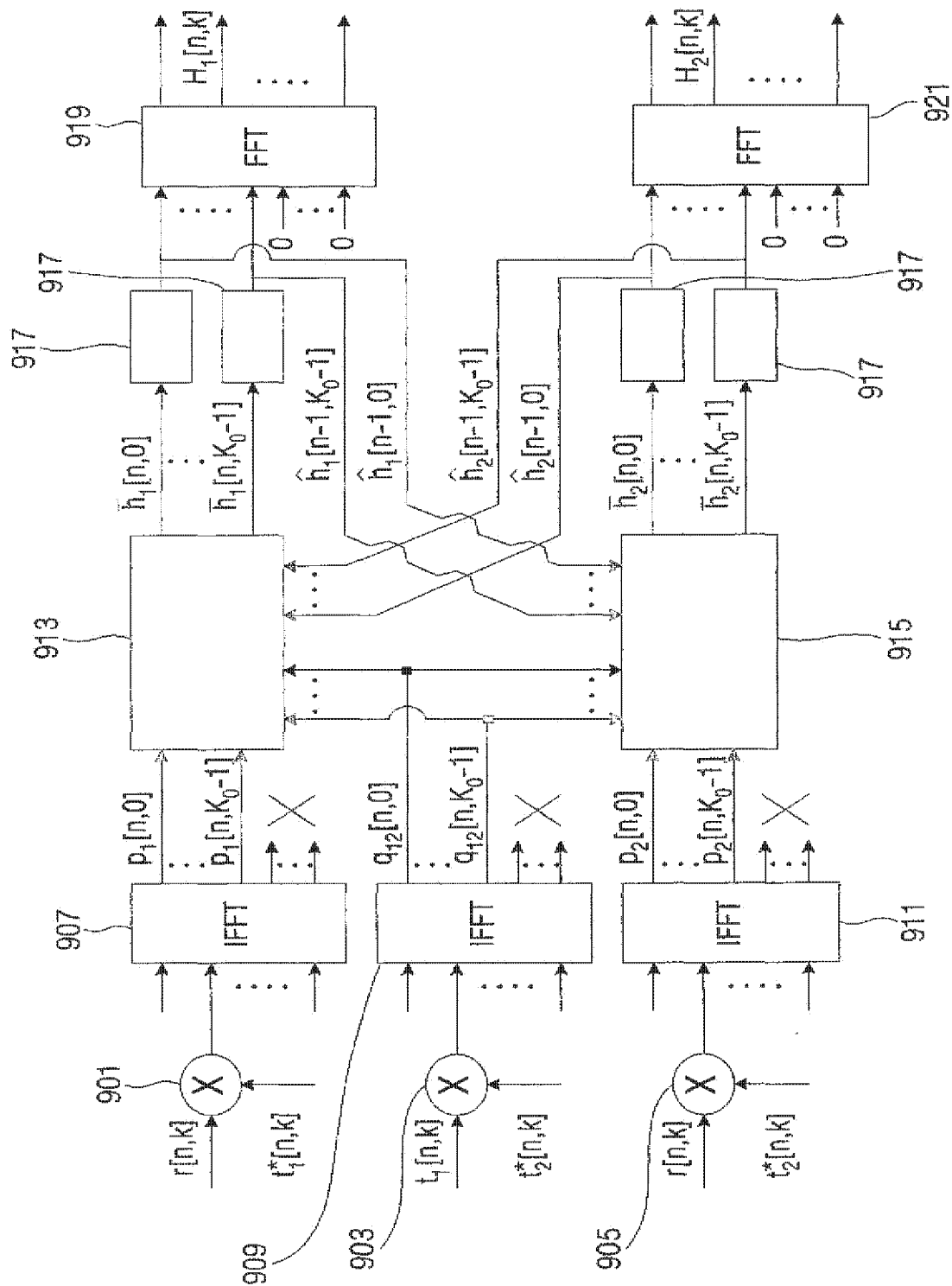


FIG. 8

# INTERNATIONAL SEARCH REPORT

International Application No.

PCT/EP 03/03211

## A. CLASSIFICATION OF SUBJECT MATTER

IPC 7 H04L27/26 H04L25/02 H04L1/06

According to International Patent Classification (IPC) or to both national classification and IPC

## B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)

IPC 7 H04L

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practical, search terms used)

EPO-Internal, INSPEC, COMPENDEX, WPI Data, PAJ

## C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category *	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X	LI Y: "SIMPLIFIED CHANNEL ESTIMATION FOR OFDM SYSTEMS WITH MULTIPLE TRANSMIT ANTENNAS" IEEE TRANSACTIONS ON WIRELESS COMMUNICATIONS, IEEE, PISCATAWAY, US, vol. 1, no. 1, January 2002 (2002-01), pages 67-75, XP001143806 ISSN: 1536-1276 cited in the application	25, 26, 28, 29
A	page 69, equation (12) figure 2  --- -/-	1-24, 27, 30

☒ Further documents are listed in the continuation of box C.

☐ Patent family members are listed in annex.

\* Special categories of cited documents:

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\*P\* document published prior to the international filing date but later than the priority date claimed

\*T\* later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention

\*X\* document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step when the document is taken alone

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Date of the actual completion of the international search

29 August 2003

Date of mailing of the international search report

10/09/2003

Name and mailing address of the ISA

European Patent Office, P.B. 5818 Patentlaan 2  
NL - 2200 HV Rijswijk  
Tel: (+31-70) 340-2040, Tx: 31 651 epo nl,  
Fax: (+31-70) 340-3016

Authorized officer

Orozco Roura, C

## INTERNATIONAL SEARCH REPORT

International Application No.

PCT/EP 03/03211

## C.(Continuation) DOCUMENTS CONSIDERED TO BE RELEVANT

Category *	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X	BARHUMI I ET AL: "Optimal training sequences for channel estimation in MIMO OFDM systems in mobile wireless channels" INTERNATIONAL ZURICH SEMINAR ON BROADBAND COMMUNICATIONS. ACCESSING, TRANSMISSION, NETWORKING, XX, XX, 19 February 2002 (2002-02-19), pages 441-446, XP010584424 cited in the application	25,26, 28,29
A	page 44-3, right-hand column	1-24,27, 30
X	WON GI JEON ET AL: "Two-dimensional MMSE channel estimation for OFDM systems with transmitter diversity" VTC FALL 2001. IEEE 54TH. VEHICULAR TECHNOLOGY CONFERENCE. PROCEEDINGS. ATLANTIC CITY, NJ, OCT. 7 - 11, 2001, IEEE VEHICULAR TECHNOLOGY CONFERENCE, NEW YORK, NY: IEEE, US, vol. 1 OF 4. CONF. 54, 7 October 2001 (2001-10-07), pages 1682-1685, XP010562250 ISBN: 0-7803-7005-8	25,26, 28,29
A	section III.B	1-24,27, 30